

Sextupole Optimization for Deflecting Cavity Scheme

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- In first order, particles traveling with non-zero vertical trajectory through a sextupole see additional skew quadrupole field
- That creates coupling between planes and therefore vertical emittance increase
- Sextupoles are located in non-zero horizontal dispersion so vertical dispersion will also be excited through skew quadrupole field
- Higher-order effects can also be important (nonlinear coupling in sextupoles)



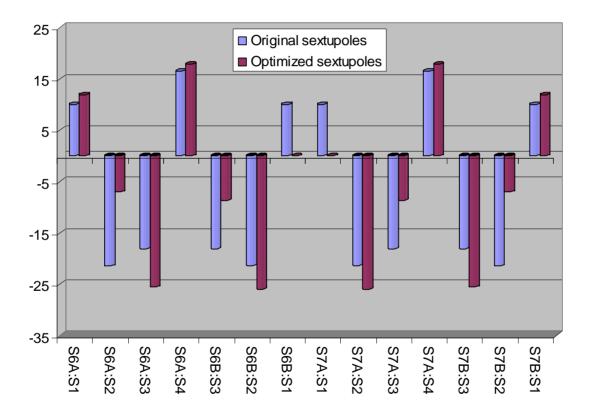


- Direct optimization based on one-pass tracking results through the deflecting section using elegant
- Constraints are:
 - Minimize vertical emittance increase
 - Compensate chromaticities to zero
- Variables are:
 - All sextupoles between cavities symmetrically around the center of the deflecting section
- Variable limits:
 - Maximum sextupole gradient is increased by 25%
 - Sextupole signs are kept constant



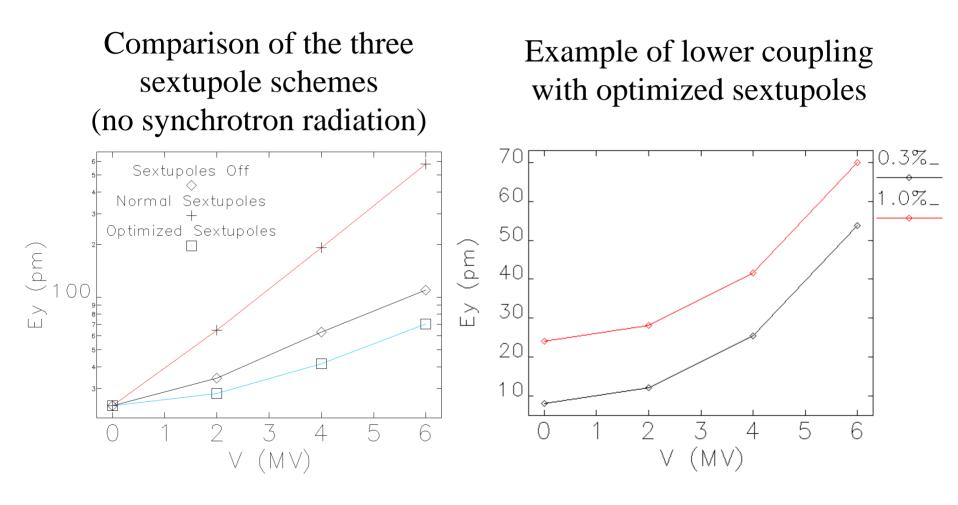


• Optimized sextupole strengths:





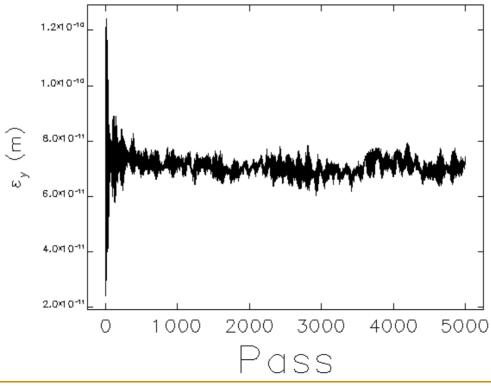








Previous studies have shown that synchrotron radiation can greatly affect the tracking results. Here we show that simulation with synchrotron radiation does not change the results.







Analysis: Coupling harmonic compensation

• The degree of emittance coupling depends on the tunes and the coupling coefficient:

$$\kappa_{q} = \frac{1}{2\pi} \int_{0}^{C} \mathbf{K}_{s} \sqrt{\beta_{x} \beta_{y}} e^{i\Psi_{q}} ds ,$$

$$\Psi_{q} = \Psi_{x} - \Psi_{y} - (\nu_{x} - \nu_{y} - q)\theta$$

- The value of coupling coefficient for the slice after 100 μrad kick for two sextupole settings:
 - Normal sextupoles:

$$\kappa_{17} = 4.6 \cdot 10^{-2}$$

- Optimized sextupoles:

 $\kappa_{17} = 1.6 \cdot 10^{-2}$





Analysis: Off-diagonal matrix elements

• We define transformation matrix between cavities as follows:

$$M = \begin{pmatrix} M_{xx} & M_{xy} \\ M_{yx} & M_{yy} \end{pmatrix}$$

- Coupling can be quantified by the determinant of M_{xy} :
 - Normal sextupoles: $M_{xy} = 4.6 \cdot 10^{-4}$
 - Optimized sextupoles:

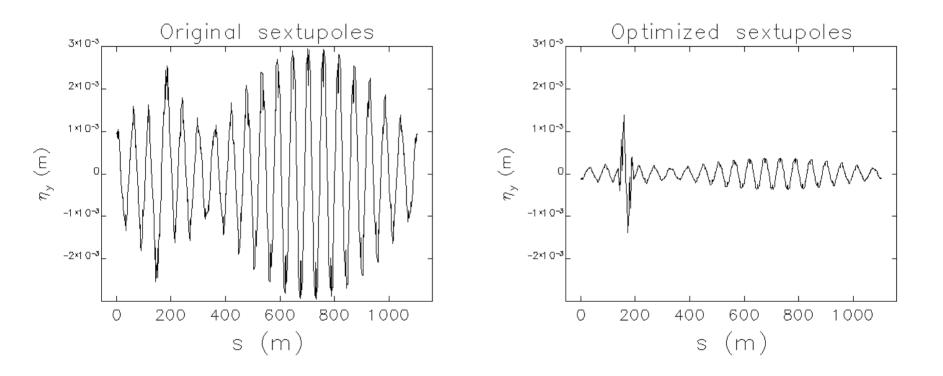
$$\left| M_{xy} \right| = 4.6 \cdot 10^{-4}$$

 $\left| M_{xy} \right| = 8.3 \cdot 10^{-6}$





Analysis: Vertical dispersion compensation







Analysis: Tune shift with amplitude

• We define tune shift with amplitude as follows:

$$\delta v_x = C_{xx}J_x + C_{xy}J_y + o(J^2),$$

$$\delta v_y = C_{xy}J_x + C_{yy}J_y + o(J^2),$$

- When calculated for the entire ring, tune shift with amplitude does not change significantly
- Tune shift calculated for deflection section only:
 - Normal sextupoles

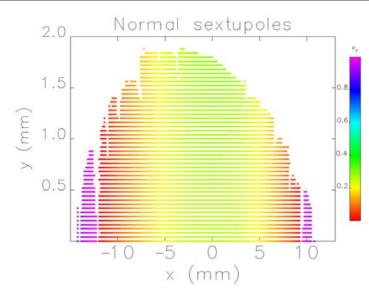
$$C_{xx} = -718 \frac{1}{m}, \quad C_{xy} = 2215 \frac{1}{m}, \quad C_{yy} = -1600 \frac{1}{m}.$$

- Optimized sextupoles

$$C_{xx} = 1960 \frac{1}{m}, \quad C_{xy} = -900 \frac{1}{m}, \quad C_{yy} = 880 \frac{1}{m}.$$

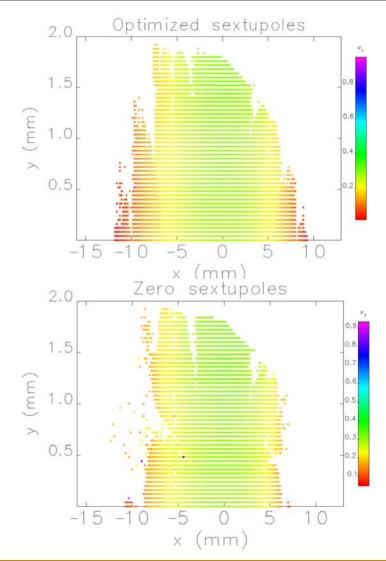


Dynamic aperture comparison



Lattice without errors 500 turns tracking

Color indicates vertical tune







Expansion to more than 2 sectors

 Optimization of sextupoles opens possibility to increase the number of sectors that could benefit from the compression scheme

Number of sectors	Vertical emittance
2	70 pm
3	59 pm
4	41 pm

• Vertical emittance blowup is no longer a limitation. Instead, new limit would be dynamic aperture decrease





Conclusions

- Due to proper optimization of sextupole strength, the vertical emittance increase is no longer a limiting issue for this scheme.
- It seems possible to increase the number of sectors between cavities to more than two. That would require additional dynamic aperture study, which is underway.



