



17TH ADVANCED BEAM DYNAMICS WORKSHOP ON

FUTURE LIGHT SOURCES

Practical Side of In-Vacuum Undulators

H. Kitamura, RIKEN

APRIL 6-9, 1999

ARGONNE NATIONAL LABORATORY, ARGONNE, IL U.S.A.

Practical side of in-vacuum undulators

Hideo Kitamura

Harima RIKEN, SPring-8

- 1. How to realize UHV for in-vacuum undulators
without any accident**
- 2. Field correction**
- 3. Image current heating**
- ~~4. Independent tuning~~**
- 5. In-vacuum revolver undulator**

Insertion Devices at SPring-8

λ_u mm	N	$G_{\min}$ mm	$B_{\max}$ tesla	$K_{\max}$	type	Pol	installed	scheduled 2000
24	187	5.0	1.0	2.2	INV-XU	hor	1	
26	172	7.0	0.83	2.0	INV-XU	hor		1
26 52	172	5.0	1.02	2.6	INV-F8	hor/ver	1	
28	160	6.5	1.0	2.4	INV-XU	hor		1
32	140	8.0	0.83	2.3	INV-XU	hor	8	1
32	781	12	0.56	1.67	INV-XU	hor		1
36	125	7.0	0.33	1.1	INV-HU	circ		1
37	2x37	8.0	0.5	1.7	INV-VU	ver	1	
40	112	15	0.59	2.2	INV-XU	hor	1	
44 92	102 48	20 20	0.5 0.36	2.1 3.1	Rev	hor circ		1
100 200	44	30	0.74	6.9	F8	hor/ver	1	
120	16	36			HU	circ	1	
120	2x12	30		3.0	HU	circ	1	
120	37	30 (20)	0.8 (1.1)		EW	circ	1	

Total 16 6

How to realize UHV for in-vacuum undulators

without any accident

1. Coating

developed by Sumitomo Special Metal (SMC)

Cu electroplating	: NG!
Ni electroplating	: good → KEK device
TiN ion-plating	: good
Ti + TiN ion-plating	: very good → SPring-8 devices



2. Baking temperature to get UHV

Higher temperature = better vacuum
irreversible demagnetization



special PM having high coercivity
+ 24hr aging ($T_{\text{aging}} = T_{\text{baking}} + 10^{\circ}\text{C}$)

1990 KEK device

NEOMAX-30SH (SMC) $iH_c = 21\text{kOe}$

$T_{\text{baking}} = 115^{\circ}\text{C}$, $T_{\text{aging}} = 125^{\circ}\text{C}$

1995 SPring-8 devices (old)

NEOMAX-33UH (SMC) 25kOe

$T_{\text{baking}} = 125^{\circ}\text{C}$, $T_{\text{aging}} = 145^{\circ}\text{C}$

1999 SPring-8 devices (present)

NEOMAX-35EH (SMC) 25kOe

$T_{\text{baking}} = 125^{\circ}\text{C}$, $T_{\text{aging}} = 145^{\circ}\text{C}$

3. Pumping speed

As high as possible ! Don't be stingy!

4. Thermal expansion at UHV bakeout

Very long undulator

Irreversible
demagnetization (%)

$T_{\text{bake}} = 125^{\circ}\text{C}$

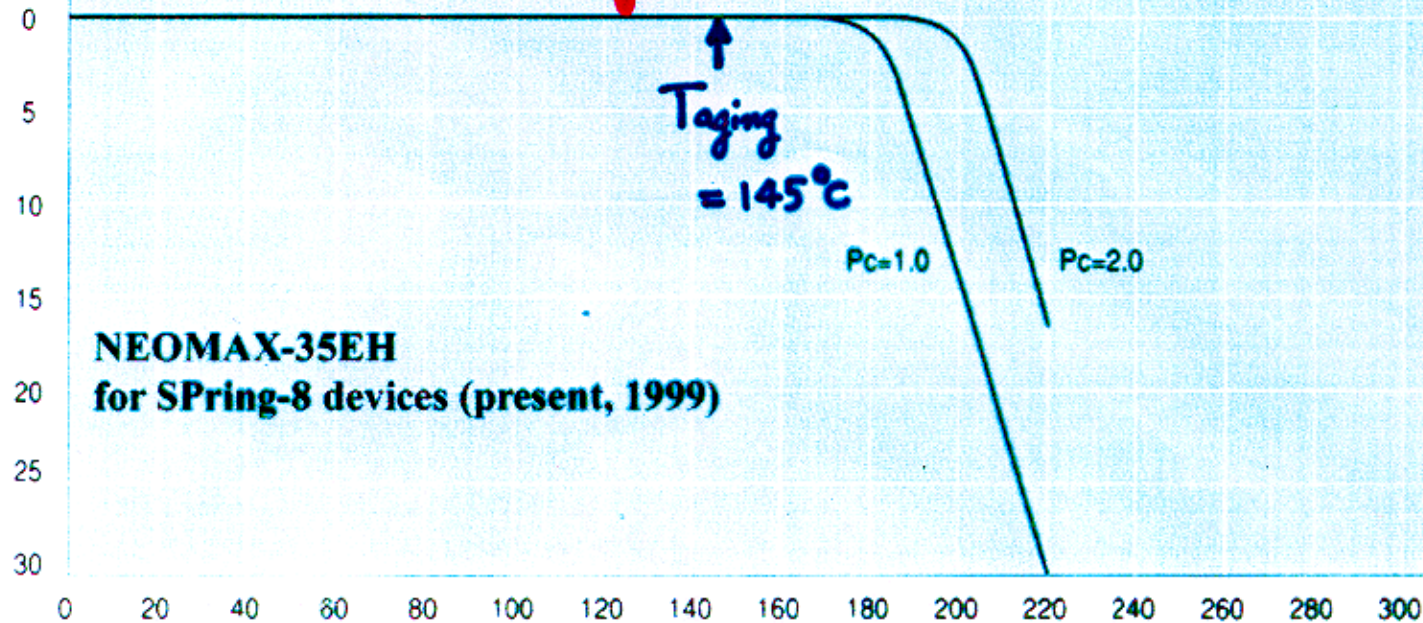
$T_{\text{aging}} = 145^{\circ}\text{C}$

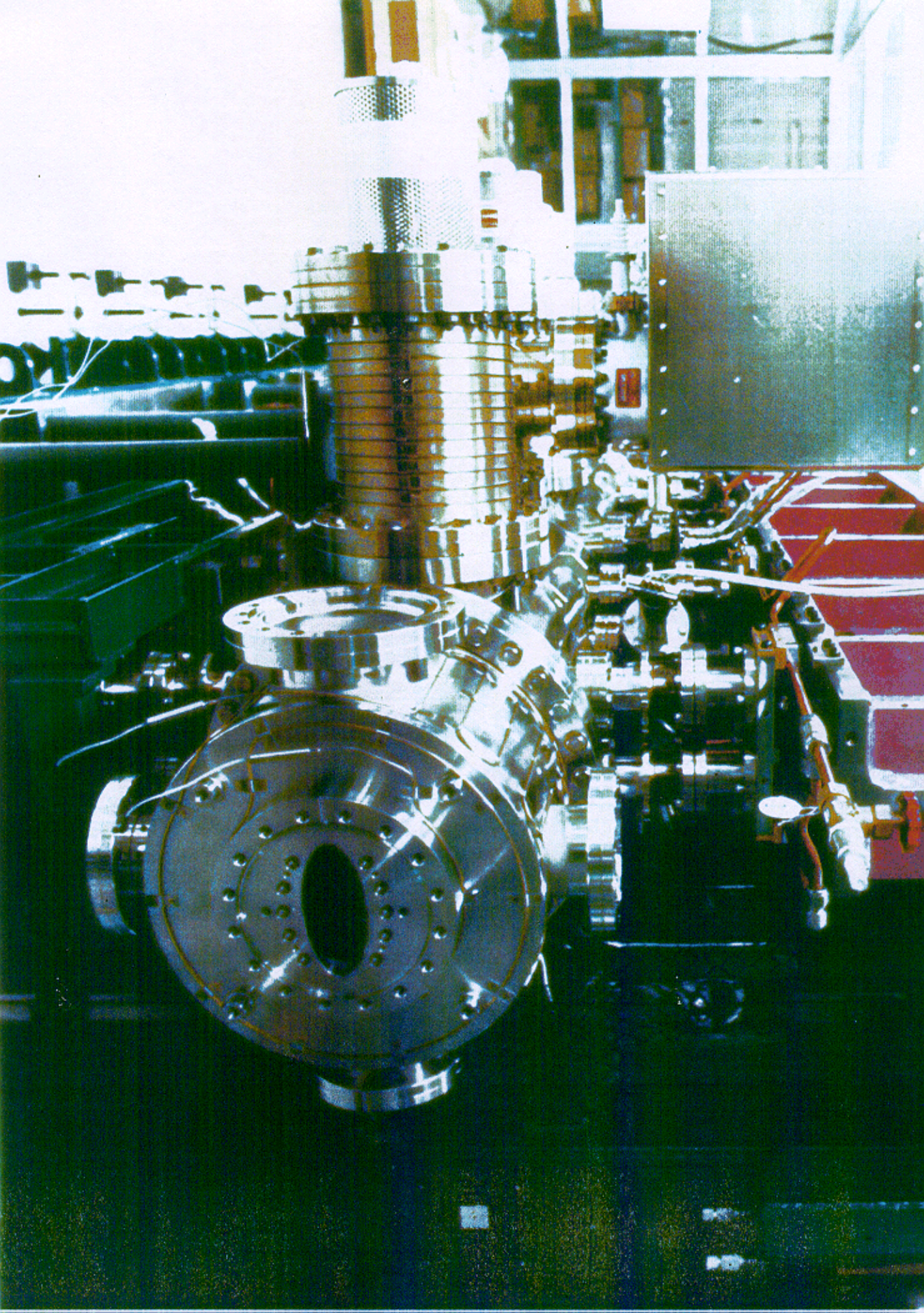
$P_c = 1.0$

$P_c = 2.0$

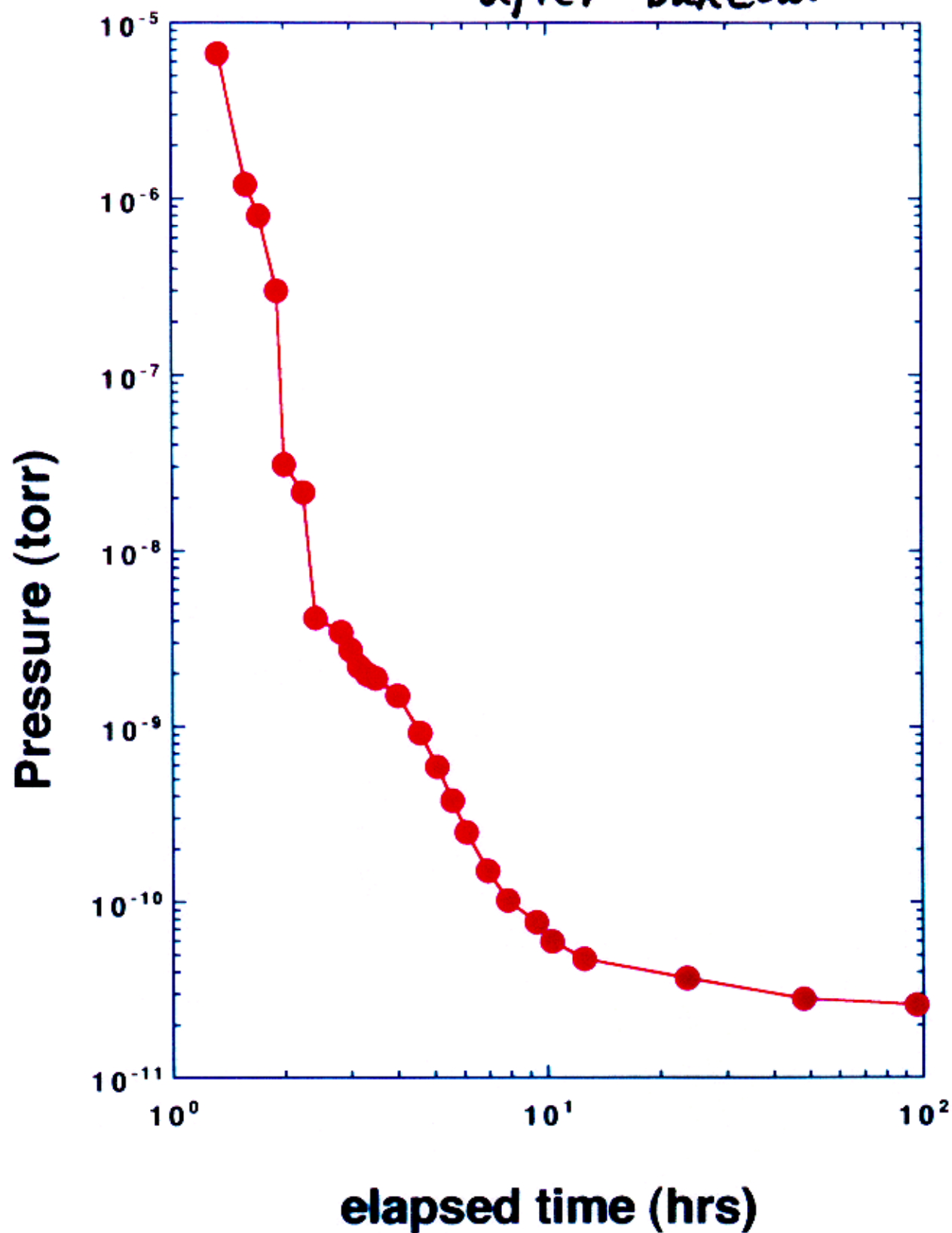
NEOMAX-35EH
for SPring-8 devices (present, 1999)

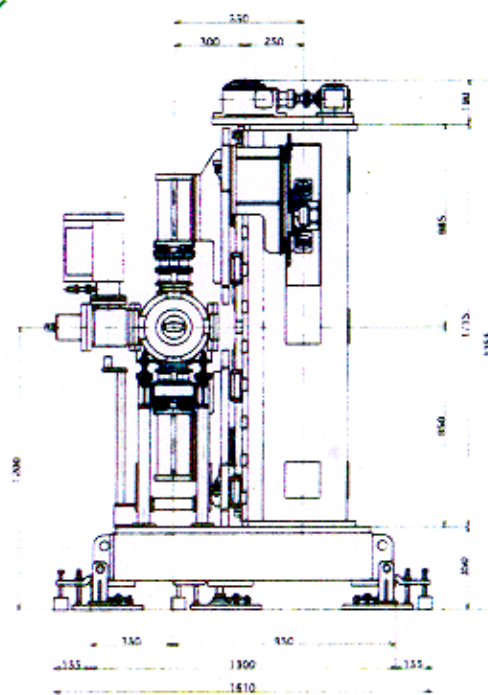
Temperature ($^{\circ}\text{C}$)





*pump down curve
after bakeout*

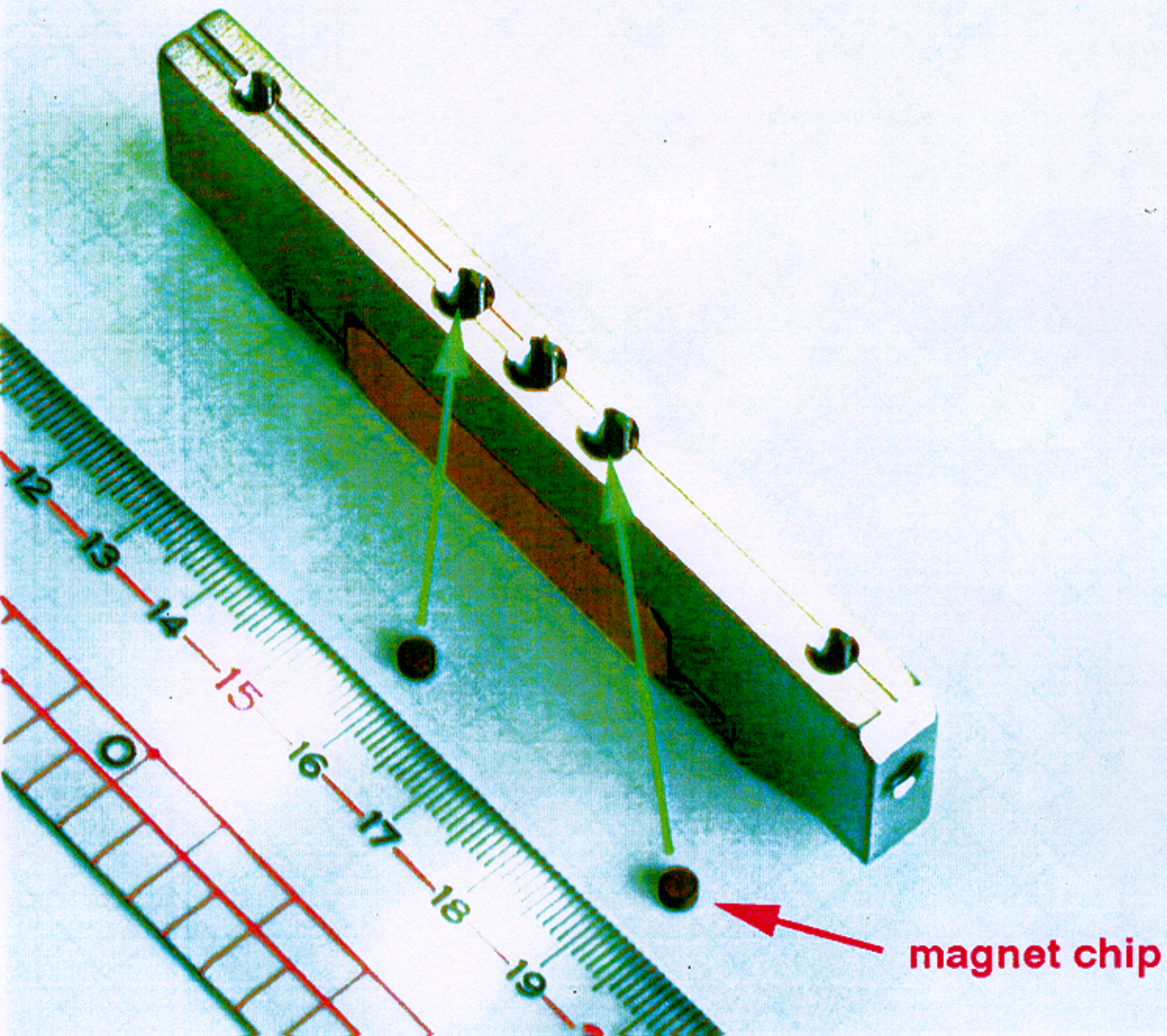


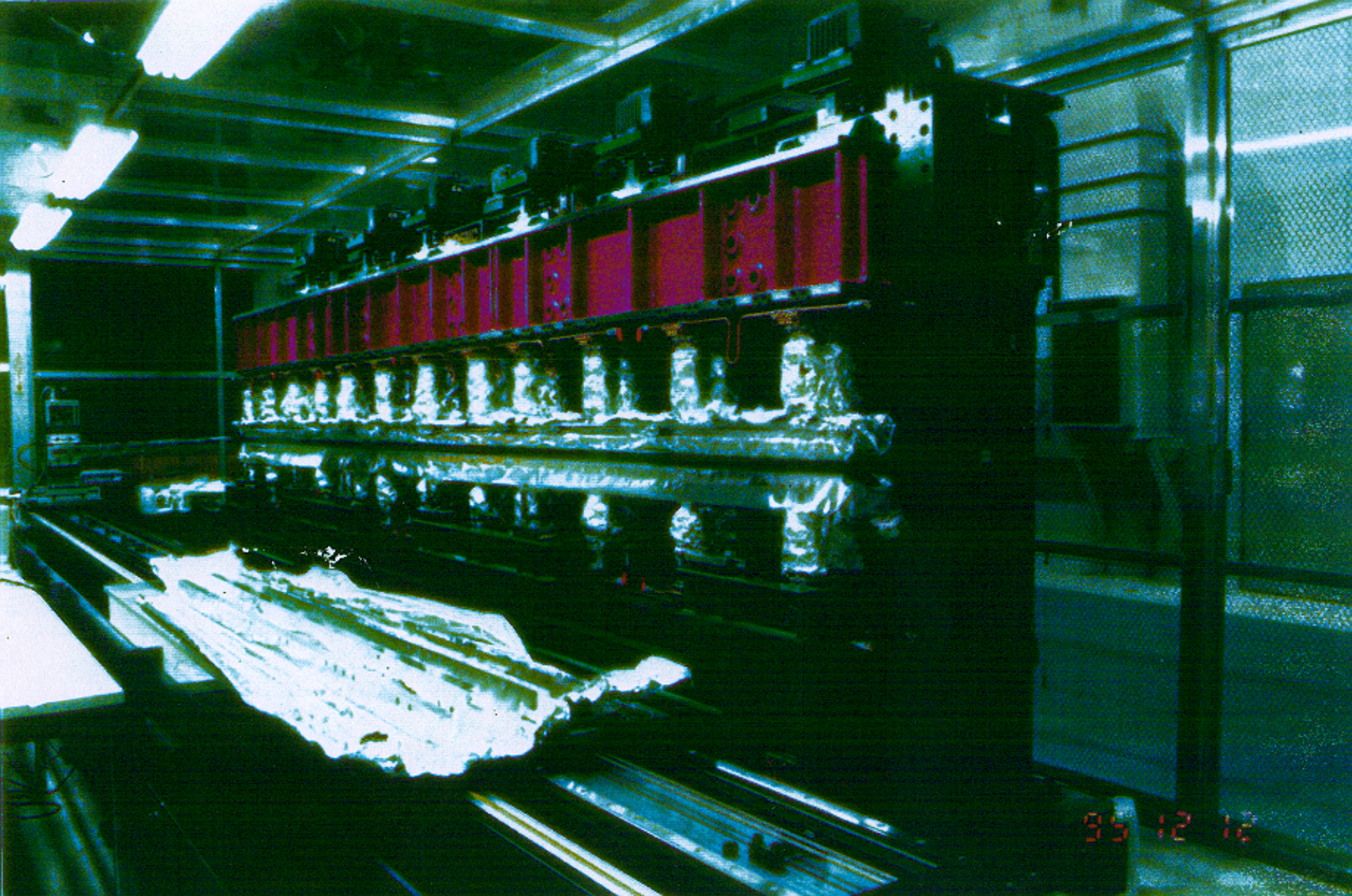
$\lambda_u = 3.2 \text{ cm}, N = 140, K_{\max} = 2.4$ 

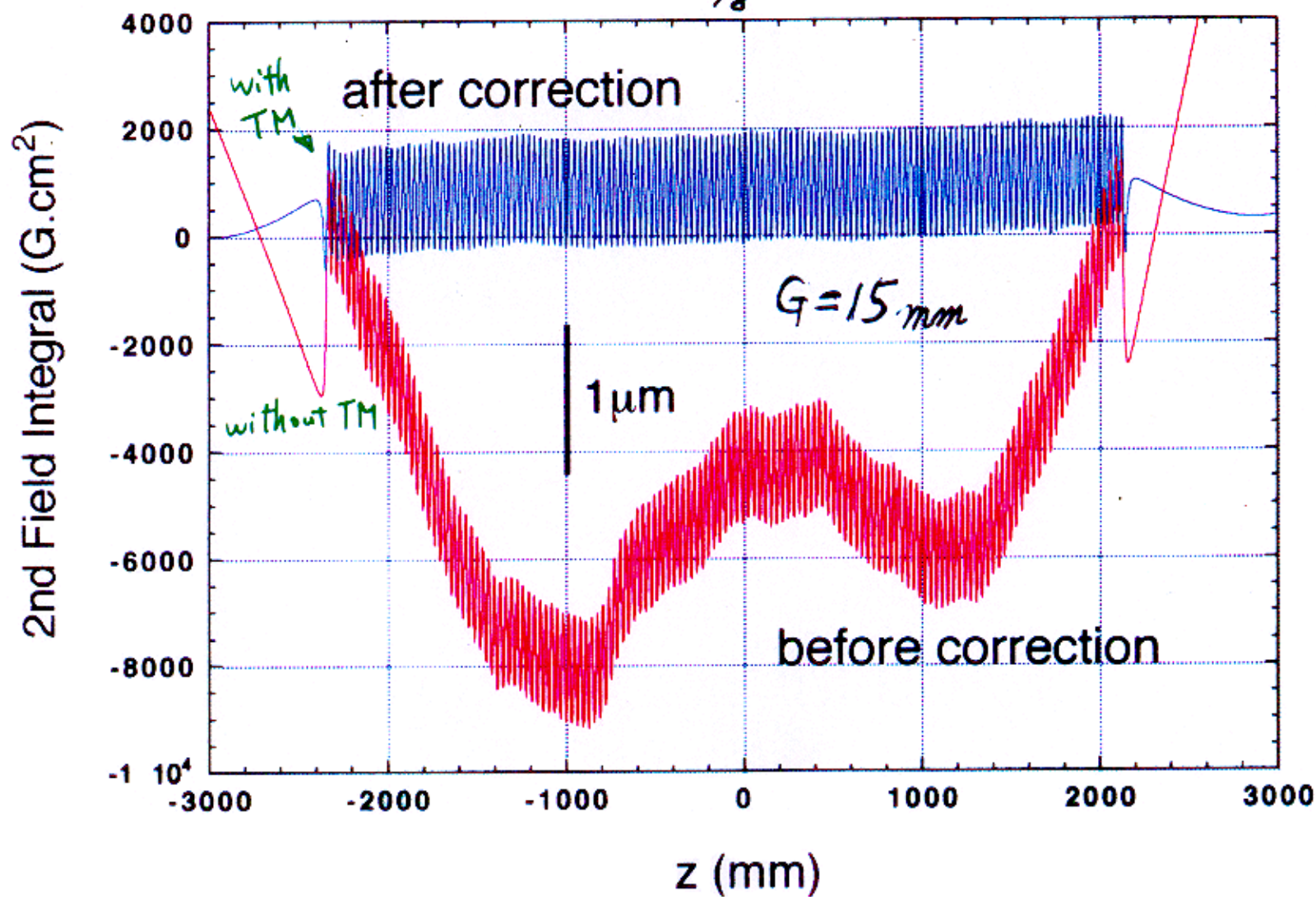
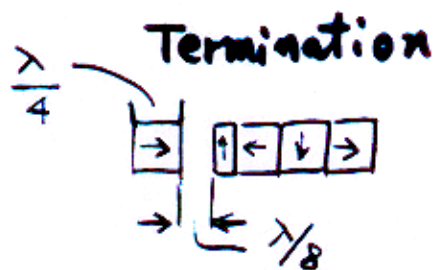
stainless
steel
(chamber)

$$T_{\text{mag}} \sim 125^\circ\text{C}$$
$$T_{\text{chamber}} \sim 200^\circ\text{C}$$

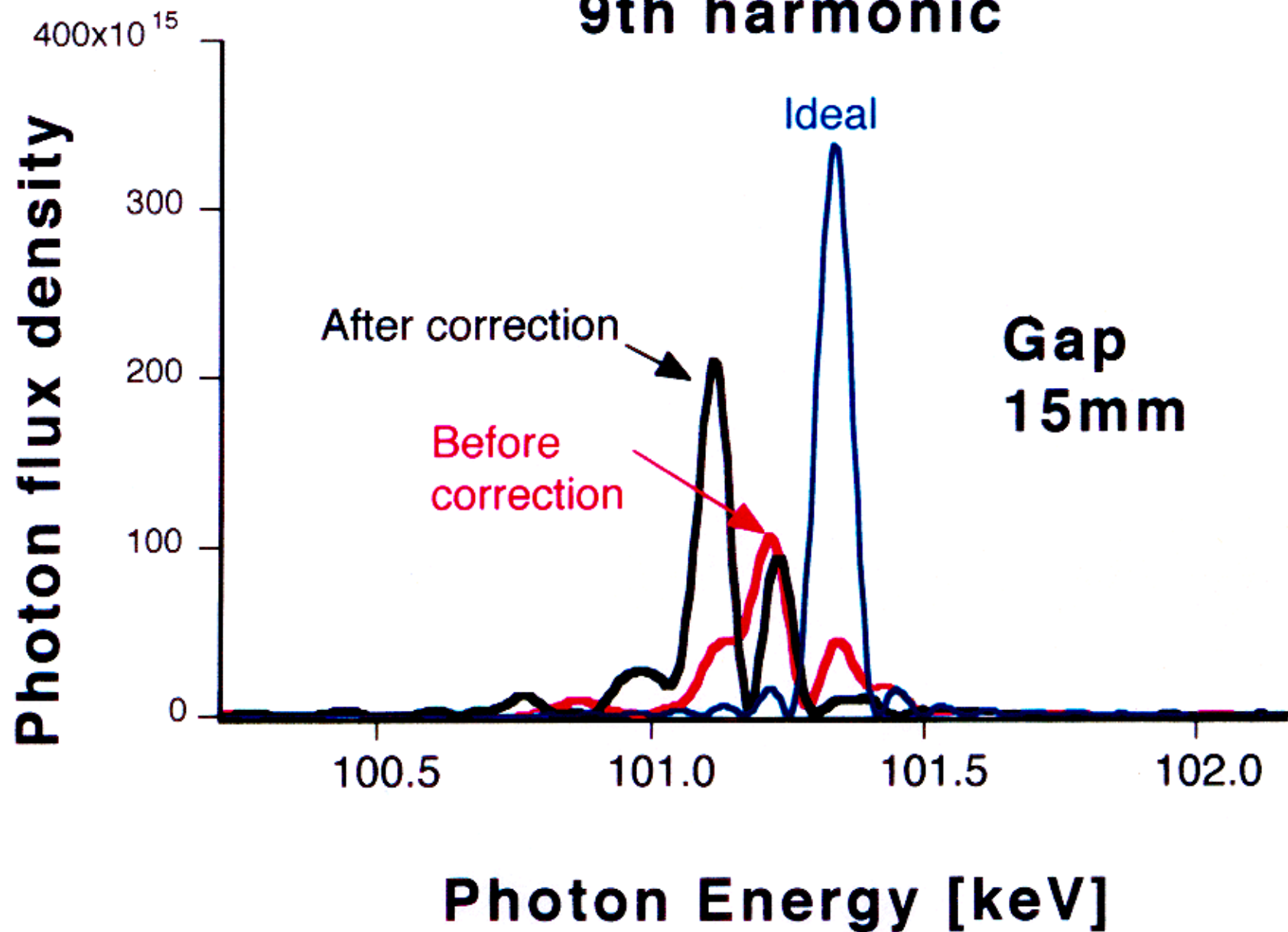
標準型真空封止X線アンジュレータ(BL09XU)

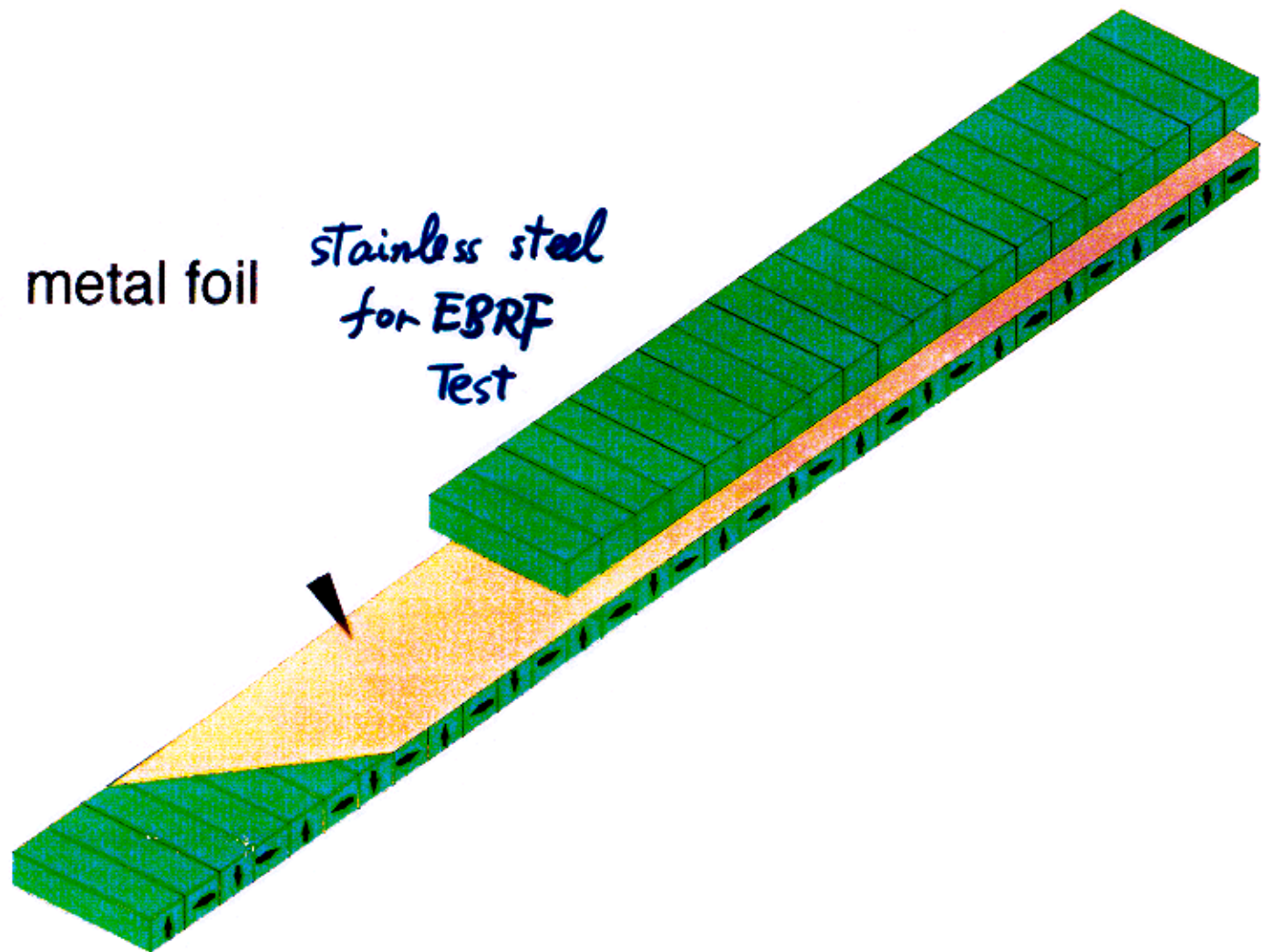


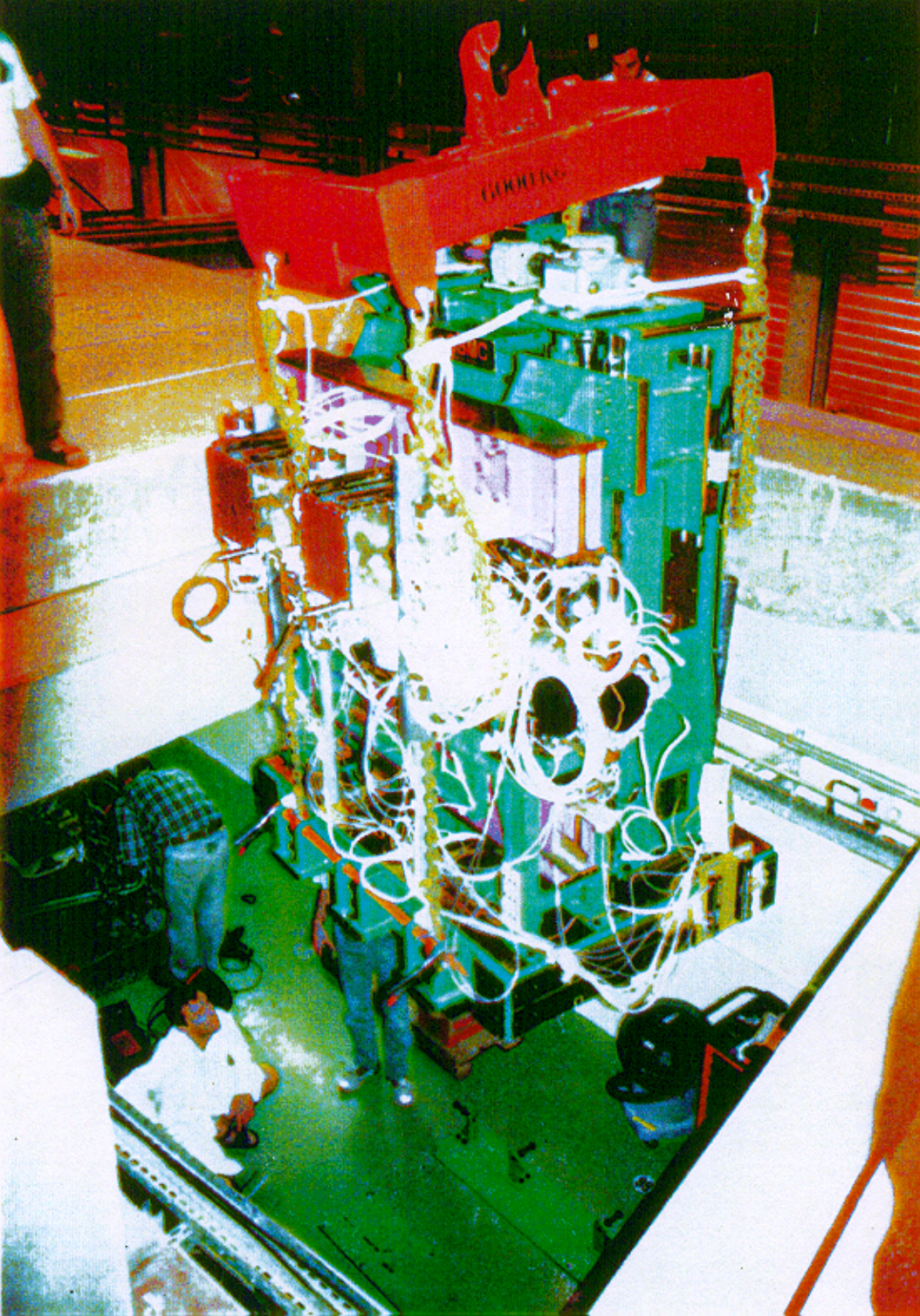


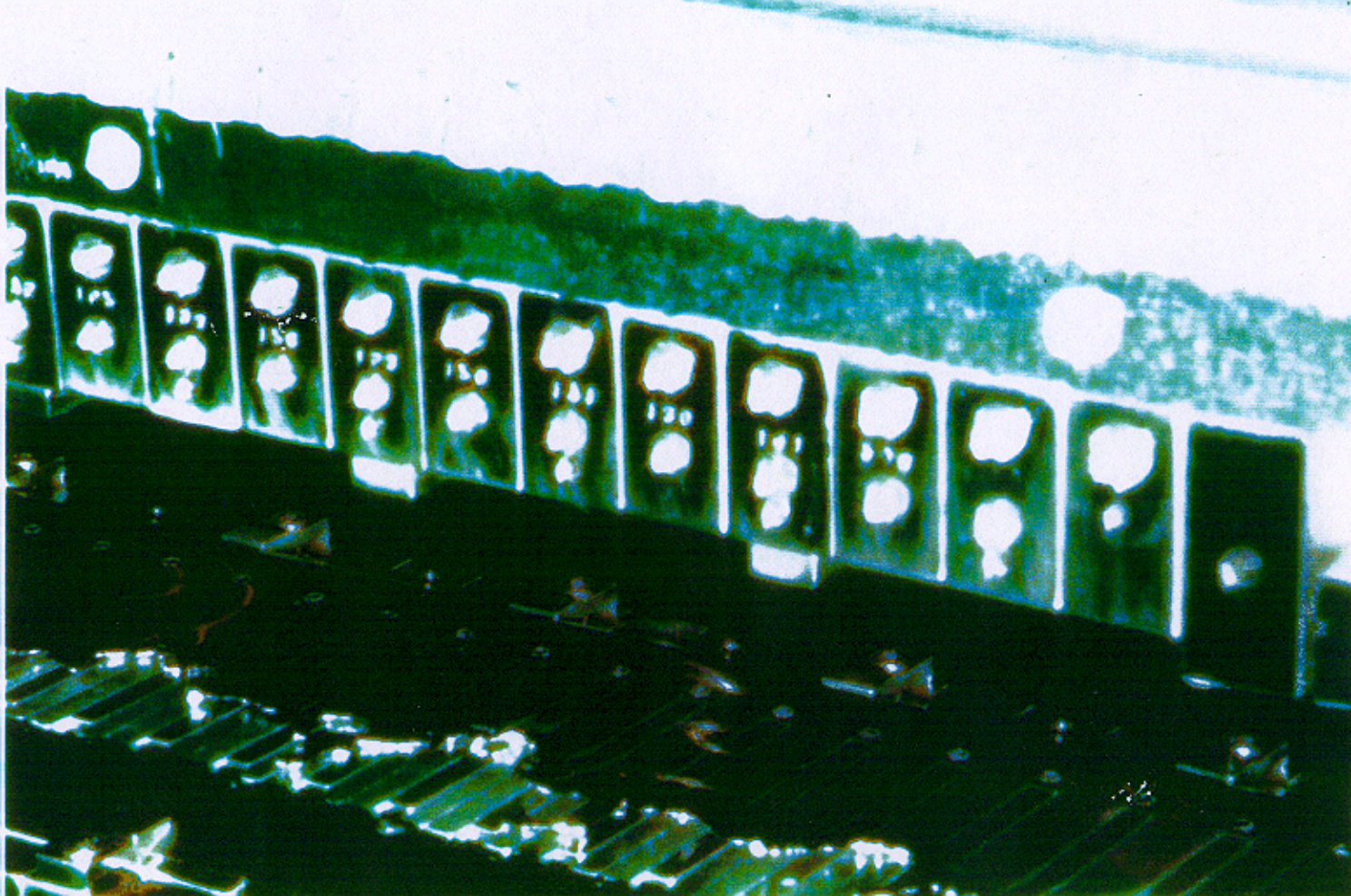


9th harmonic

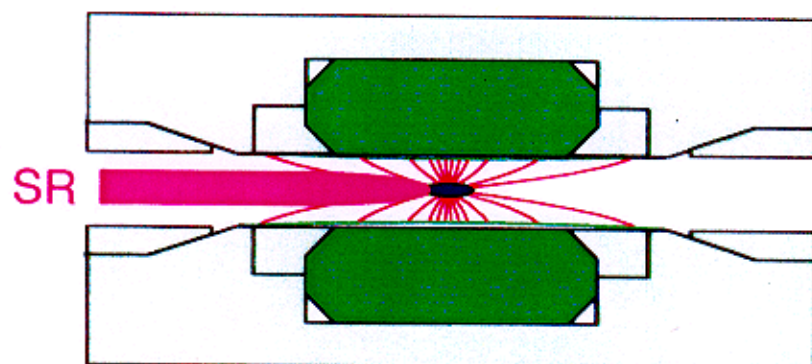




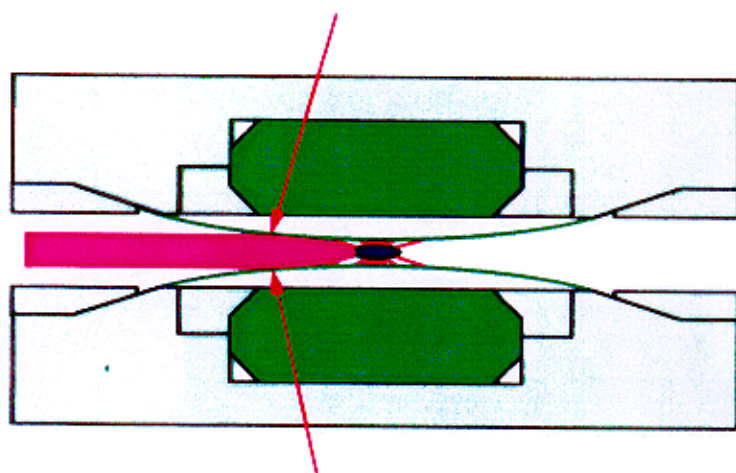




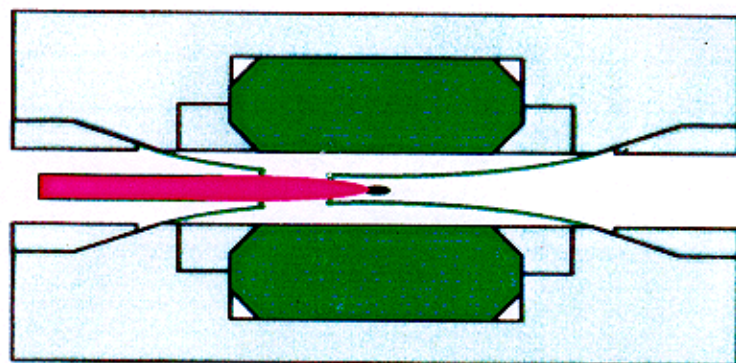
STEP 1



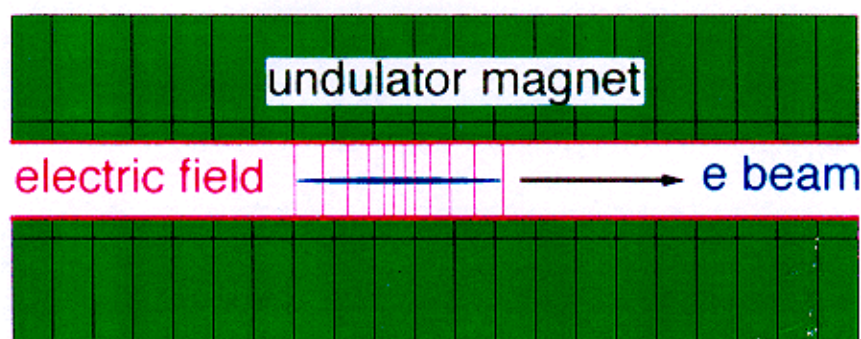
STEP 2



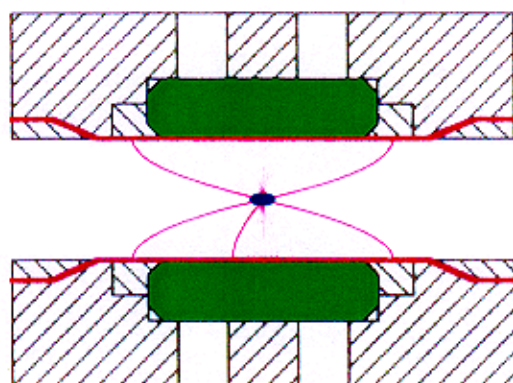
STEP 3



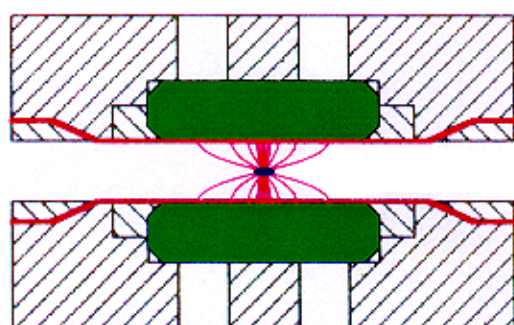
Power generated by image current



low current density



high current density



$$P = M I_b^2 \left(\frac{L_u}{\pi G} \right) \frac{\Gamma(3/4)}{\omega_o \sigma_t^{3/2}} \sqrt{\frac{\mu_o \rho}{2}}$$

- M : number of bunches
 I_b : beam current per bunch
 ρ : resistivity
 L_u : length of undulator
 G : gap
 σ_t : bunch length

Bane and
Krinsky

Metal foil

Cu : low resistivity

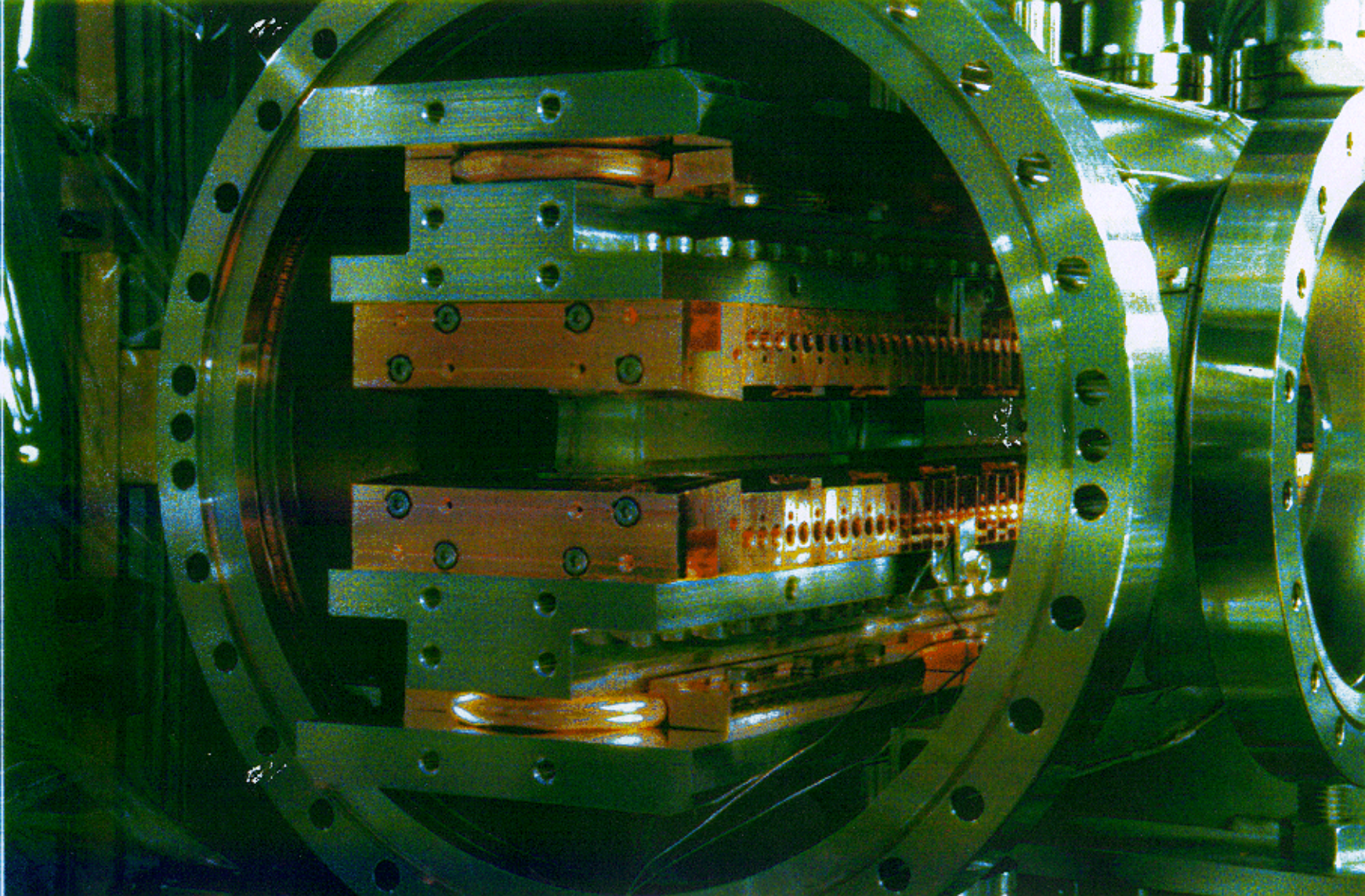
Ni : magnetic force → good thermal contact

skin depth: $< 1\mu\text{m}$

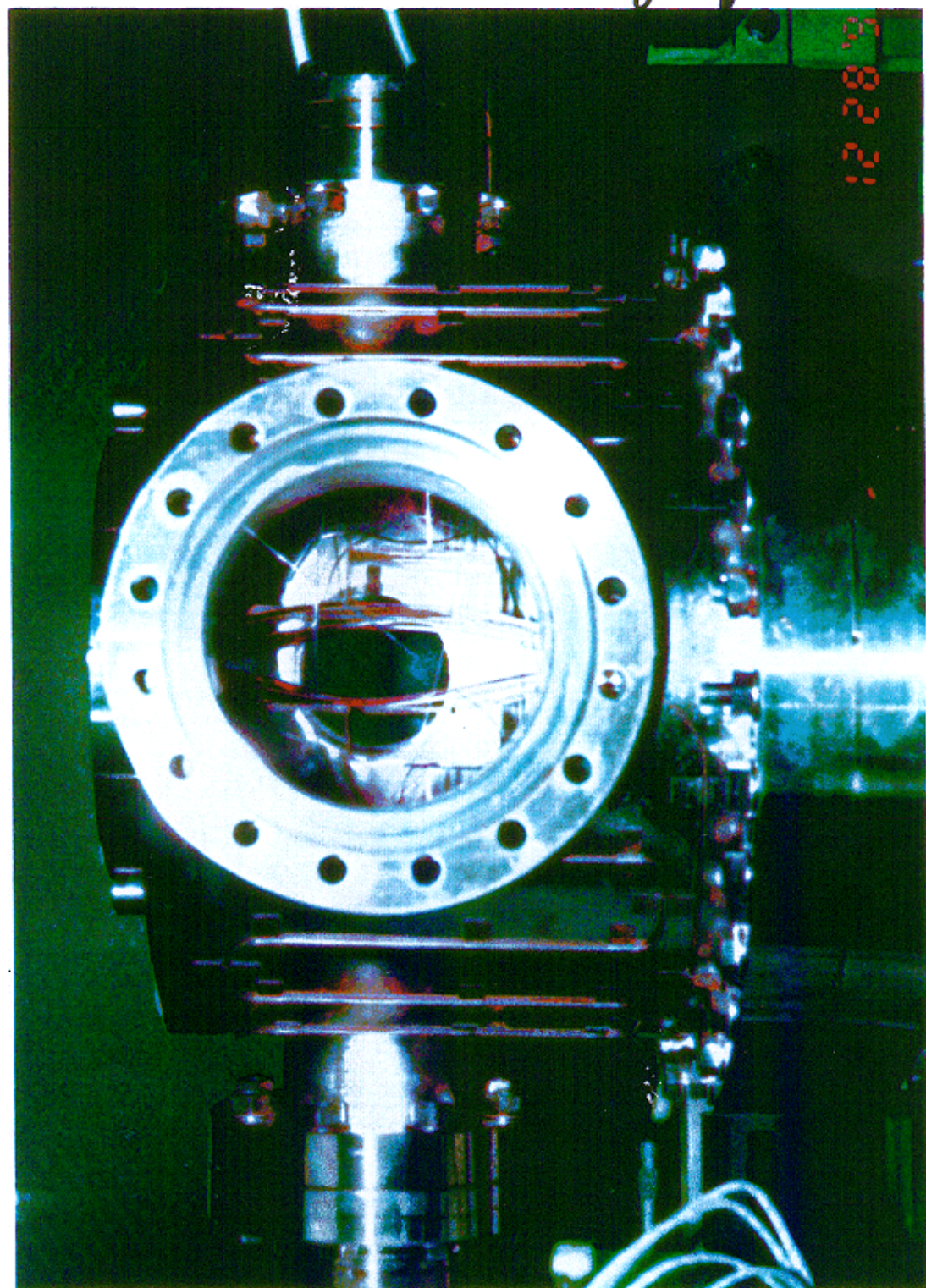
Ni ($50\mu\text{m}$) + Cu ($10\mu\text{m}$)

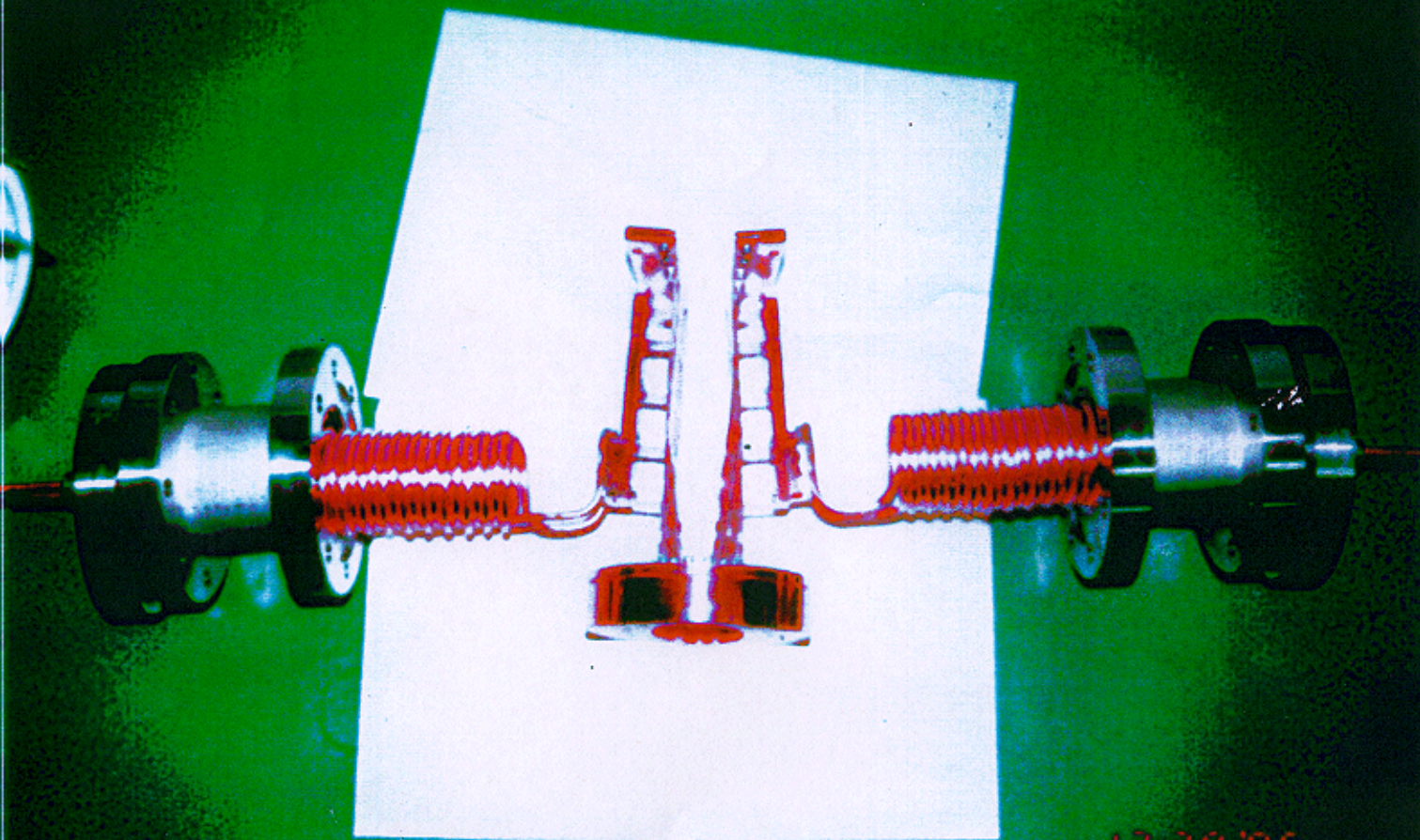


magnetic flux loss : $< 0.1\%$ ($\lambda_u = 32\text{mm}$)



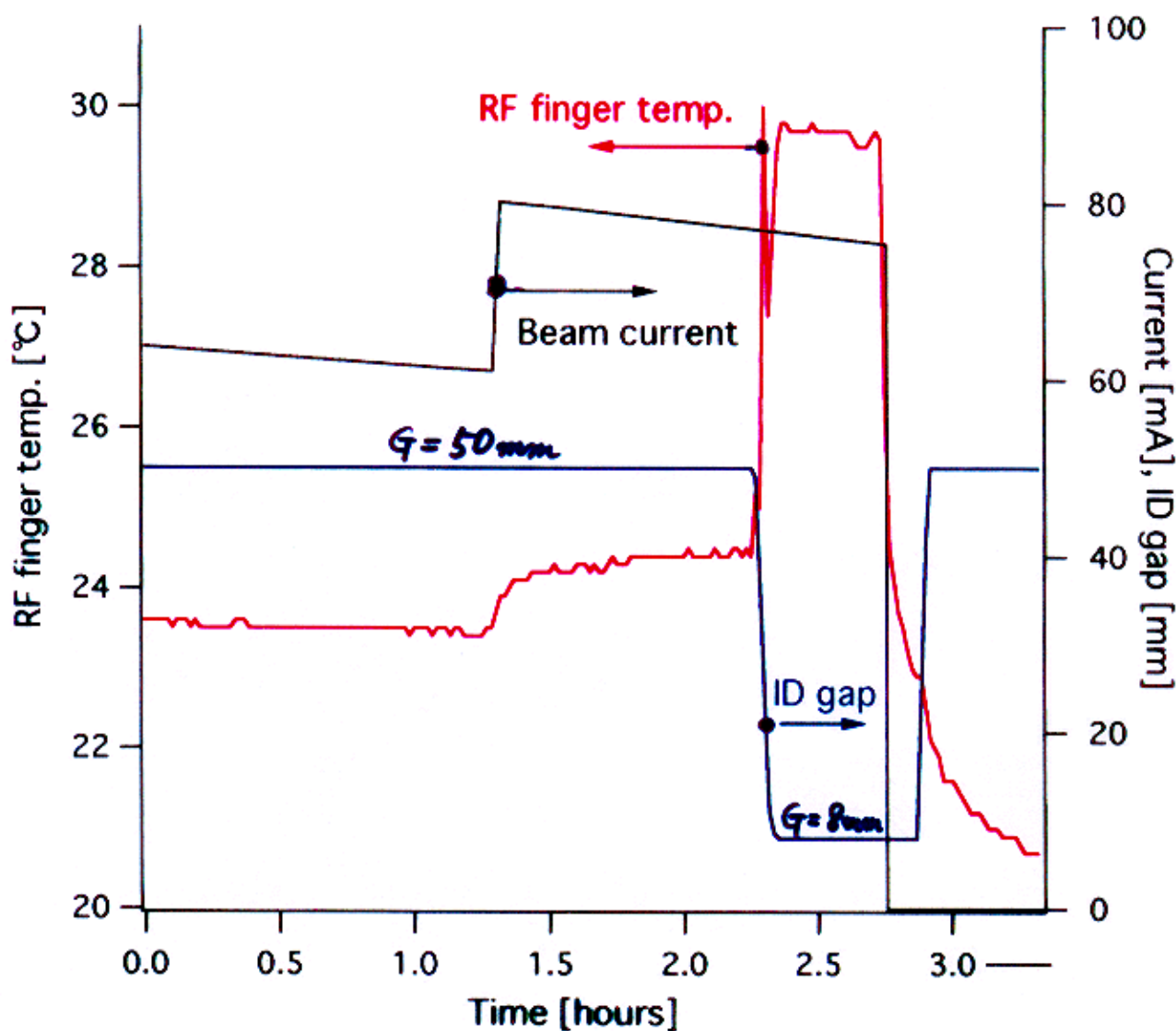
rf-finger (old type)
without water cooling system





12/28/96

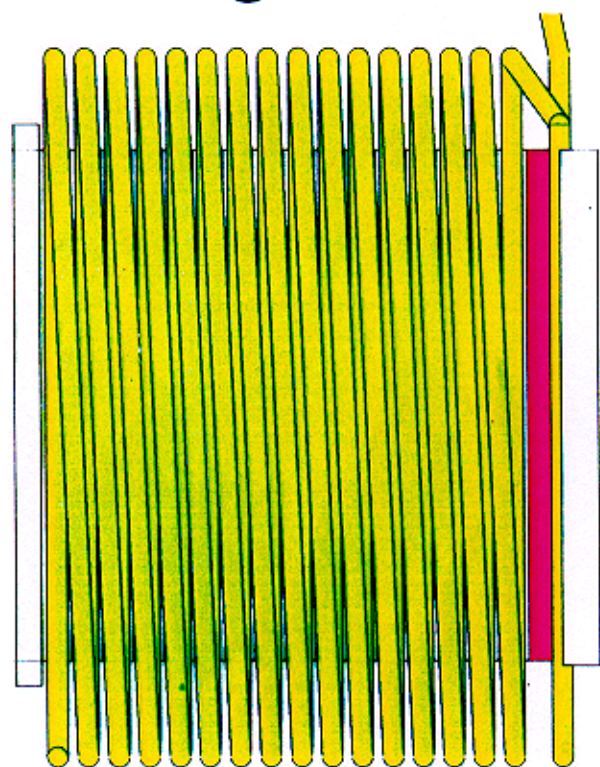
at Spring-8



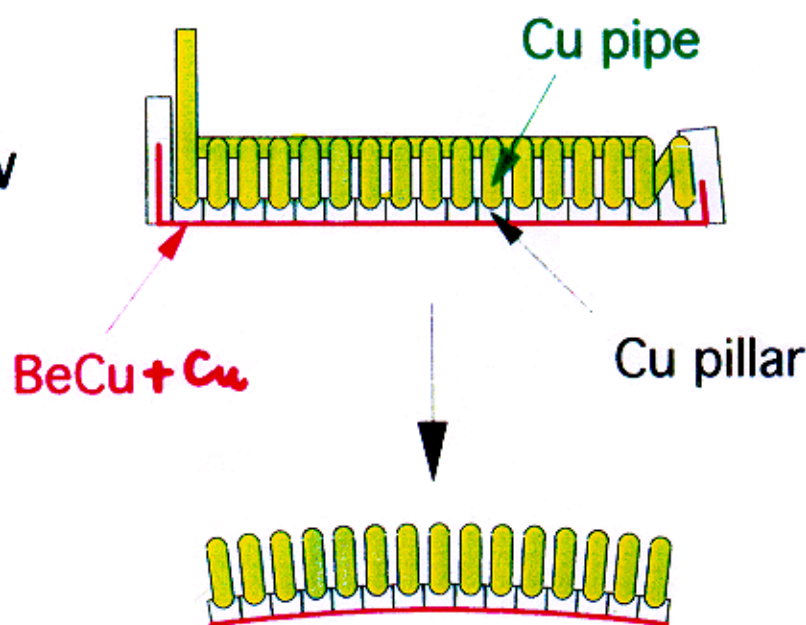
SPring-8 ID39 transition temperature
Undulator entrance, upside
(1/6 filling, 98/06/11)

Water cooling system for flexible rf-finger

top view



side view



In-vacuum Revolver Undulators (mini gap)

R&D study at SPring-8

Characteristics

1. Four different period lengths

$$\lambda_u = 6, 10, 15, 20 \text{ mm}$$

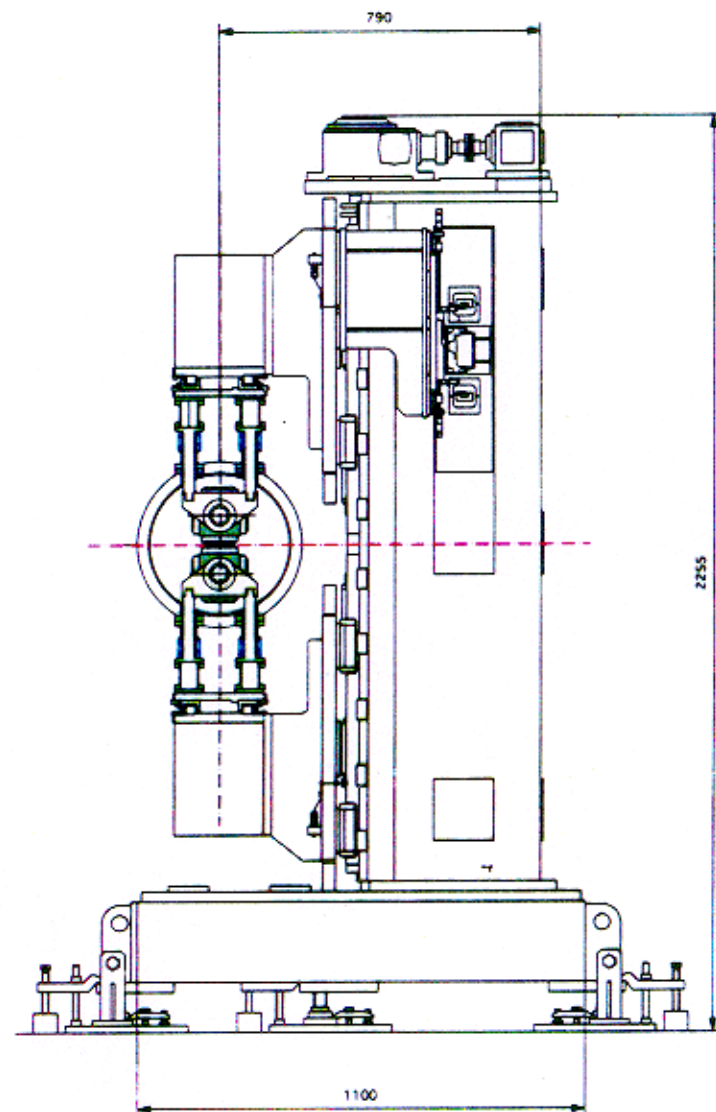
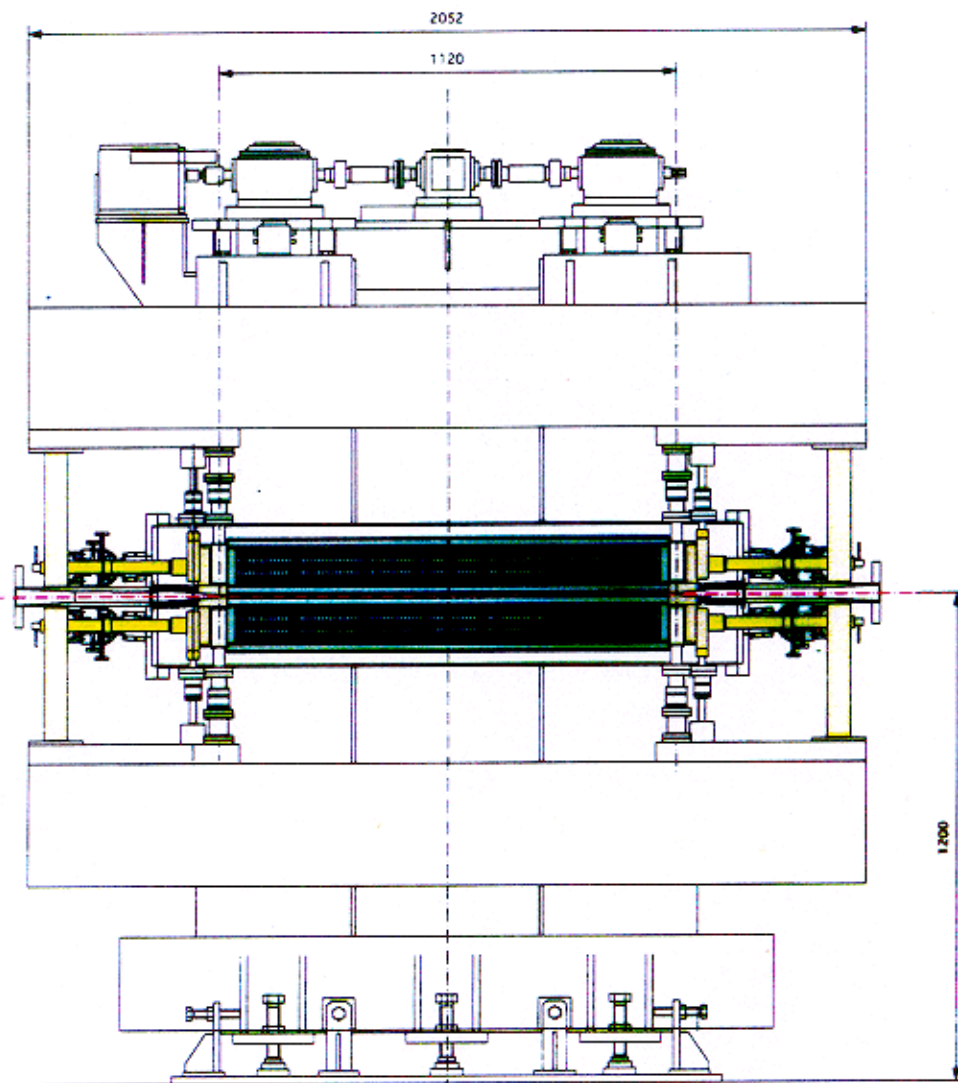
2. $L = 1 \text{ m}$

3. $G_{\min} = 2 \text{ mm}$

4. Detachable/attachable flexible rf finger

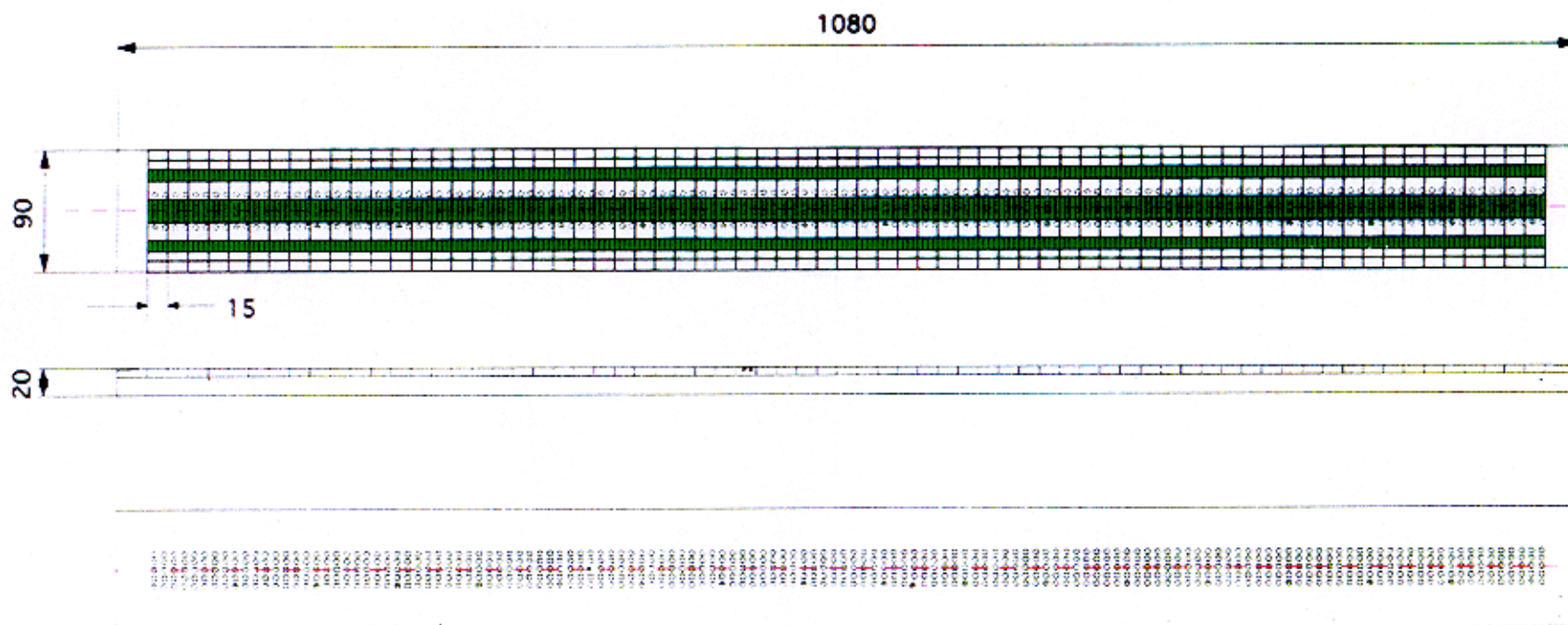
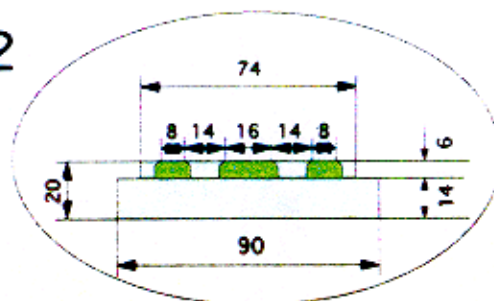
5. Net load minimized by additional magnetic arrays to obtain repulsive force

6. Two-stage differential pumping system for feedthrough rotatable axes.



In-vacuum Revolver Undulator

x2



Top view

side

back

magnet array for $\lambda_u = 15 \text{ mm}$

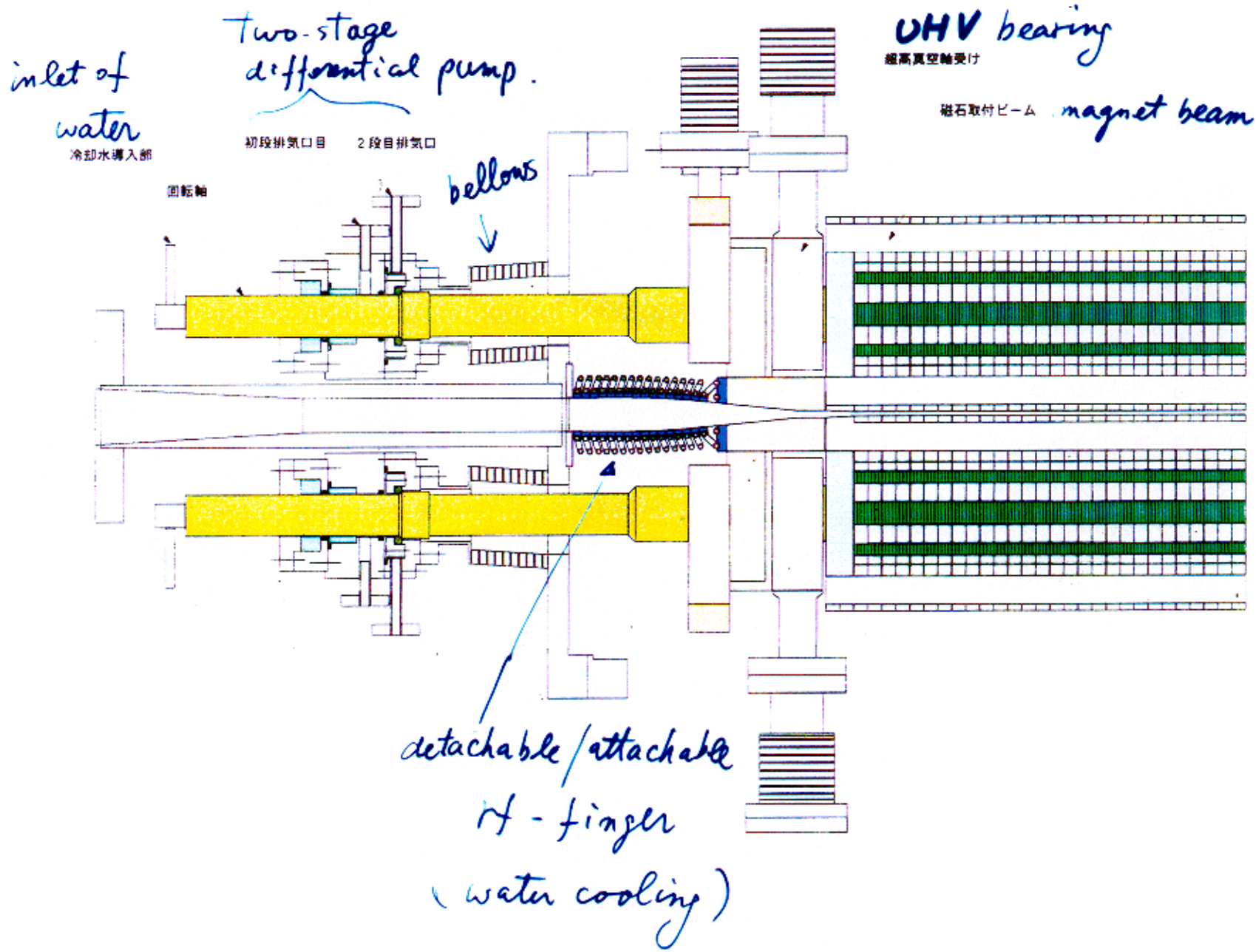
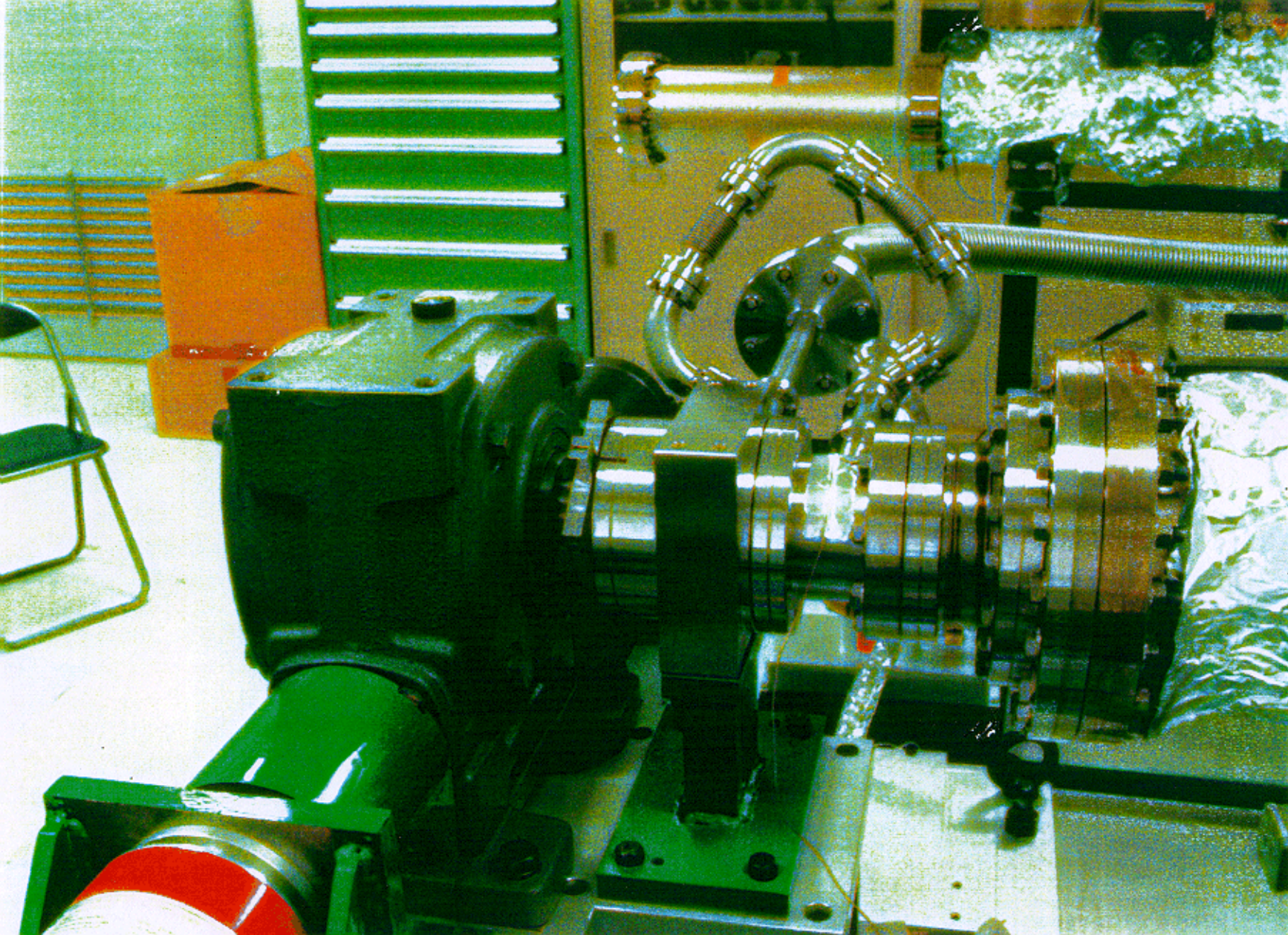
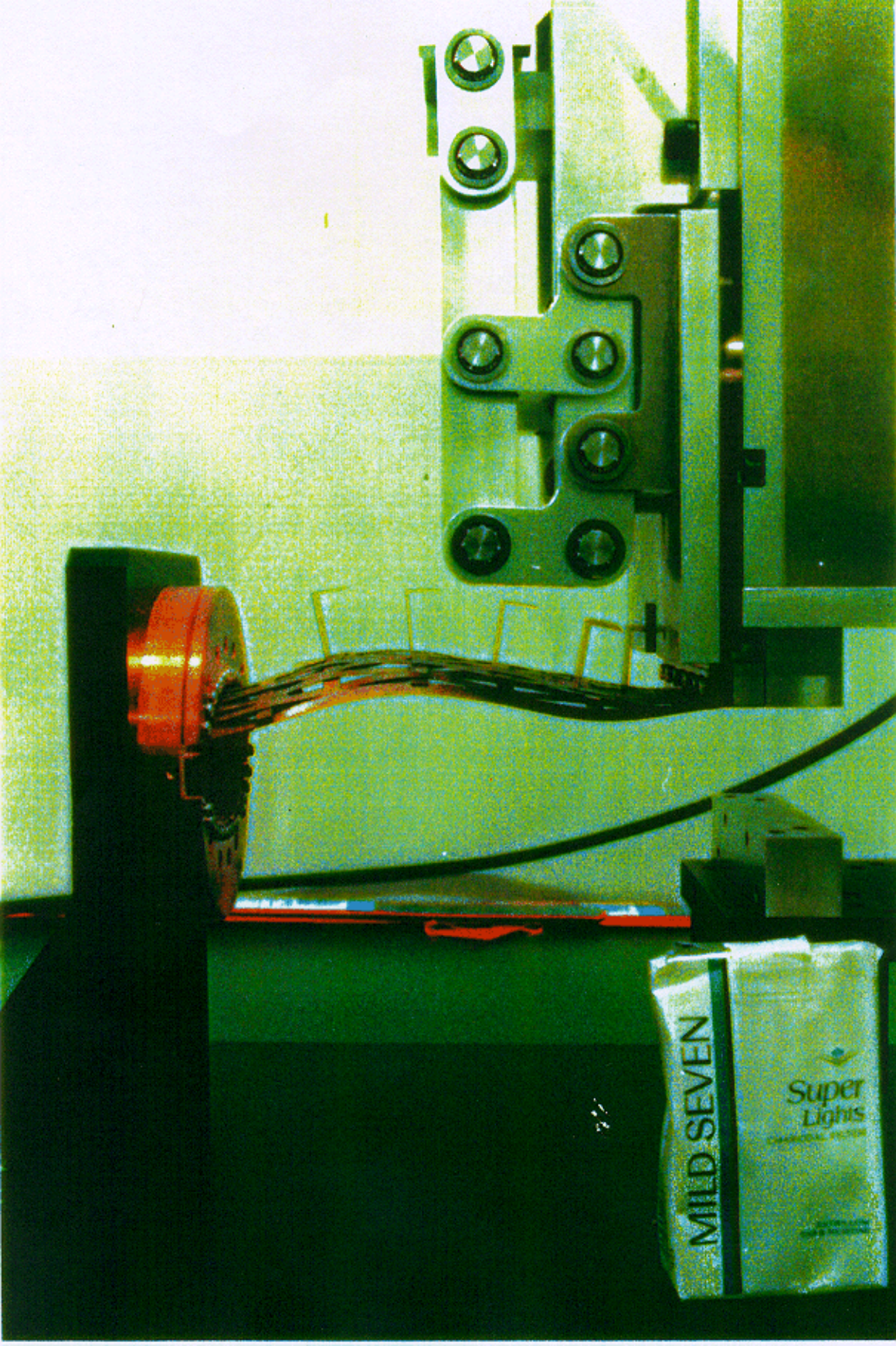


図4-1-7 回転導入部







MILD SEVEN

Super
Lights
CHARCOAL FILTER