

Parameter Optimization for a 1.5 to 0.15 nm FEL for a Very Low Slice Emittance

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- Slice Emittance
- Optimization Algorithm
- FEL Optimization Results
- Comparison with Simulation
- Sensitivities to Parameter Changes

Analytical 3D FEL Formula

Ming Xie, LBNL, determined universal FEL scaling by fitting numerical solutions of the coupled Maxwell-Vlasov equations that describe the FEL interactions.

$$\eta = 0.35 \eta_d^{0.57} + 0.55 \eta_\epsilon^{1.6} + 3 \eta_\gamma^2 + 0.35 \eta_\epsilon^{2.9} \eta_\gamma^{2.4} + 51 \eta_d^{0.95} \eta_\gamma^3 + 5.4 \eta_d^{0.7} \eta_\epsilon^{1.9} + 1140 \eta_d^{2.2} \eta_\epsilon^{2.9} \eta_\gamma^{3.2}$$

The scaling parameters

$$\eta_d = \frac{L_{1d}}{L_R}, \quad \eta_\epsilon = \left(\frac{L_{1d}}{\beta_{xy}} \right) \left(\frac{4\pi\epsilon_n}{\gamma_r \lambda_r} \right); \quad \eta_\gamma = 4\pi \left(\frac{L_{1d}}{\lambda_u} \right) \left(\frac{\sigma_E}{E_o} \right)$$

measure the deviation of the beam from the 1-D case.

$$L_{G3D} = (1 + \eta) L_{G1D}; \quad P_{sat} \approx \frac{1.6 \rho}{(1 + \eta)^2} P_{beam};$$

$$L_{sat} \approx \log\left(\frac{P_{sat}}{\rho \gamma m_e c^2 \Delta \omega} \right) L_{G3D}$$

1D FEL Formulae

1D Power Gain Length:

$$L_{G1D} = \frac{\lambda_u}{4\pi\sqrt{3}\rho}$$

Pierce Parameter:

$$\rho = \frac{1}{4} \left(\frac{a_w}{4\gamma} \frac{\Omega_p}{\omega_u} F_1 \right)^{\frac{2}{3}}$$

Bessel Function Term:

Helical: $F_1 = 1$

Linear: $F_1 = J_0(\xi/2) - J_1(\xi/2)$

$$\xi = \frac{a_w^2}{1 + a_w^2}$$

Undulator Wavenumber:

$$k_u = \frac{2\pi}{\lambda_u} \qquad \omega_u = k_u c$$

1D FEL Formulae

Undulator Parameter:

$$K = \frac{B_u c}{k_u (m_e c^2 / e)}$$

Undulator Strength:

Helical: $a_w = K$

Linear: $a_w = K / \sqrt{2}$

β -Function for Natural Focusing:

$$\beta_{nat} = \sqrt{2} \frac{\gamma}{K k_u}$$

Total Betatron Wavenumber:

$$k_\beta = \sqrt{\left(\frac{1}{\beta_{ext}}\right)^2 + \left(\frac{1}{\beta_{nat}} r_{kxkw}\right)^2}$$

Total β -Function:

$$\beta_{xy} = \frac{1}{k_\beta}$$

1D FEL Formulae

Raleigh Range:

$$L_R = \frac{\pi w_o^2}{\lambda_r}$$

Optical Waste Size:

$$w_o = \sqrt{2} \sqrt{\sigma_{xy}^2 + 2 \frac{\lambda_r L_{G1D}}{(4\pi)^2}}$$

Plasma Frequency:

$$\Omega_p = \sqrt{\frac{4\pi r_e c^2 n_e}{\gamma}}$$

Electron Density:

$$n_e = \frac{I_{pk}}{2\pi \sigma_{xy}^2 e c}$$

RMS Electron Beam Size:

$$\sigma_{xy} = \sqrt{\frac{\epsilon_n}{\gamma} \beta_{xy}}$$

1D FEL Formulae

Resonant Condition:

$$\lambda_r = \frac{\lambda_u}{2 \gamma^2} (1 + a_w^2)$$

Classical Electron Radius:

$$r_e = \frac{e c^2}{(m_e c^2 / e)} 10^{-7}$$

Frequency Spread:

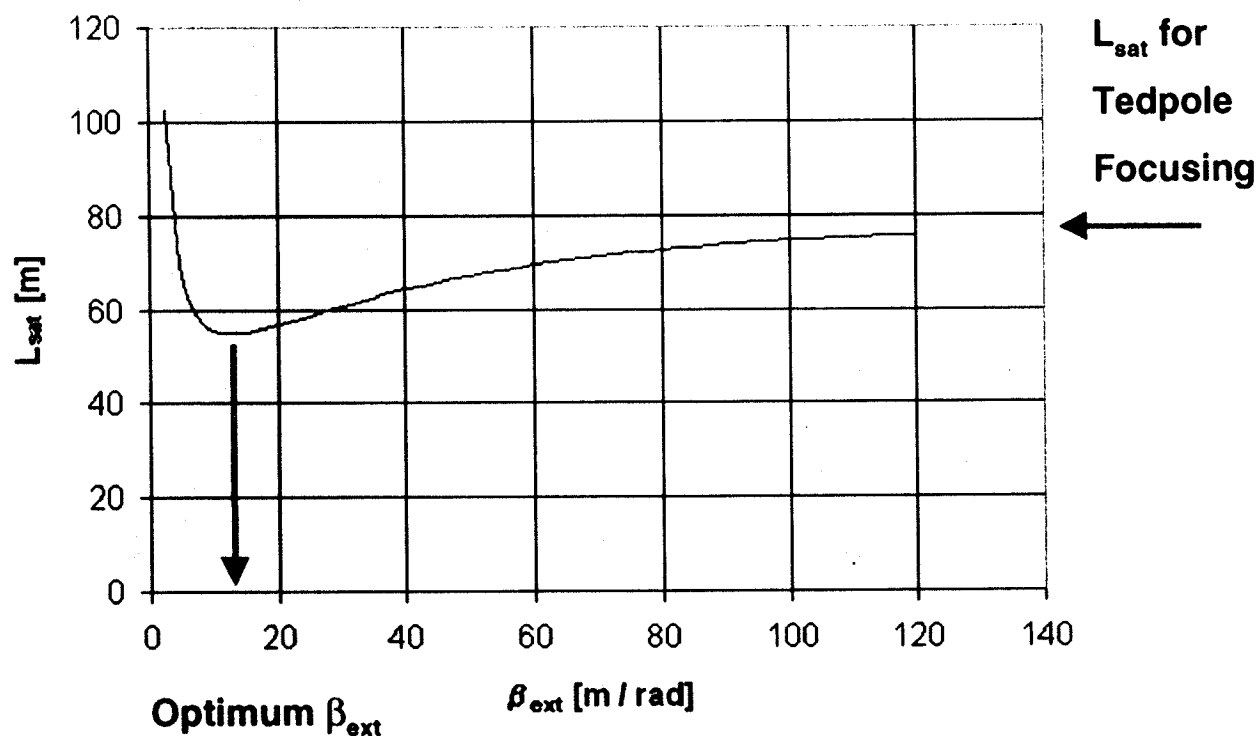
$$\Delta \omega = 2 \frac{c}{\lambda_r} \frac{\Delta \gamma}{\gamma}$$

Parameters and Constants:

λ_r	Resonant Wavelength
γ_r	Resonant Energy
$\Delta \gamma / \gamma$	Energy Spread
ϵ_n	Normalized Emittance
λ_u	Undulator Period
B_u	Peak On-Axis Undulator Field
β_{ext}	External Focusing Strength
I_{pk}	Peak Bunch Current
m_e	Electron Mass
c	Speed of Light
e	Electron Charge

Optimum Focusing

FEL Optimization



$$\lambda_r = 0.15 \text{ nm}$$

$$\lambda_u = 2.7 \text{ cm}$$

$$I_{\text{pk}} = 3400 \text{ A}$$

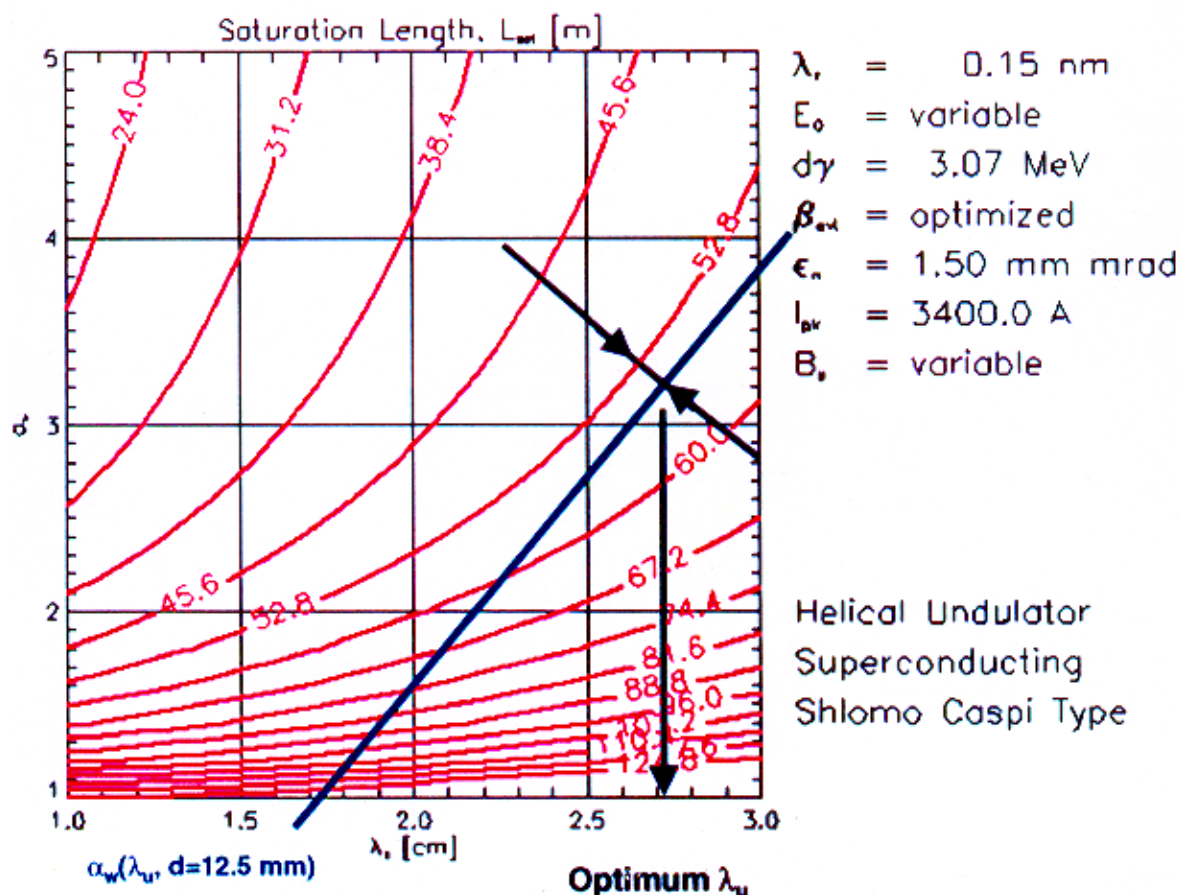
$$\varepsilon_n = 1.5 \text{ mm mrad}$$

Helical Undulator

Optimum Period

Optimum period exists for constant diameter or gap.

FEL Optimization



Based on: M. Xie, PAC95, p. 183 (1996)

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FEL Parameter Classification

- **Case Variables**
 - λ_r
 - gap / diameter
 - undulator type
 - $d\gamma$
- **Optimized Variables**
 - λ_u
 - β_{ext}
- **Free Variables**
 - γ_r
 - a_w
 - B_u
- **Plot Variables (vs. $I_{\text{pk}}, \epsilon_n$)**
 - $\lambda_r, \gamma_r, a_w, B_u, L_{\text{sat}}, P_{\text{sat}}$

FEL Optimization Cases

- Wavelengths Range
 $\lambda_r = 0.1, 0.15, 1.5, 15 \text{ nm}$
- Fixed Energy Spread
 $d\gamma = 6$

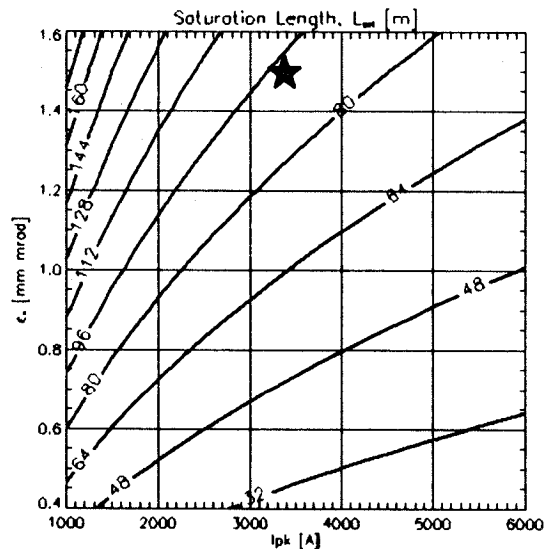
Undulator Type	Gap / Diameter	Quad. Foc. , β_{ext}
	[mm]	
linear	6	optimized
linear	6	none
linear	7	optimized
linear	7	none
helical	10	optimized
helical	10	none
helical	12.5	optimized
helical	12.5	none

Optimization Results - L_{sat}

FEL Optimization

$\lambda_r = 0.15 \text{ nm}$
linear

★ LCLS

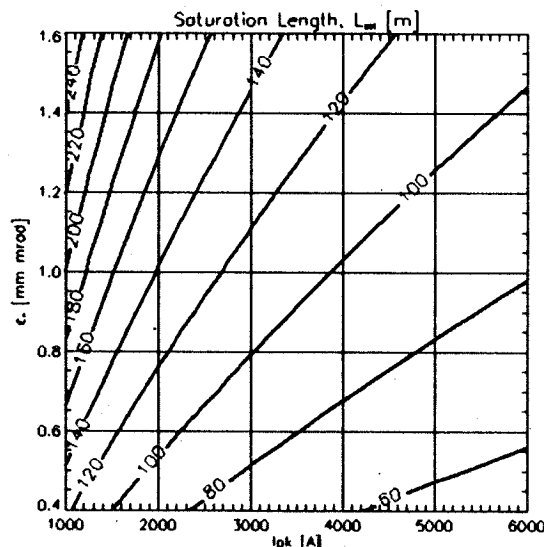


$\lambda_r = 0.15 \text{ nm}$
 $E_0 = \text{variable}$
 $dE = 3.07 \text{ MeV}$
 $\beta_{\text{ext}} = \text{optimized}$
 $\lambda_w = \text{optimized}$
 $\alpha_w = \text{variable}$
 $B_w = \text{variable}$
gap = 6.00 mm

Based on: M. Xie, PAC95, p. 183 (1996)

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FEL Optimization



$\lambda_r = 0.15 \text{ nm}$
 $E_0 = \text{variable}$
 $dE = 3.07 \text{ MeV}$
 $\beta_{\text{ext}} = \text{none}$
 $\lambda_w = \text{optimized}$
 $\alpha_w = \text{variable}$
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gap = 6.00 mm

Based on: M. Xie, PAC95, p. 183 (1996)

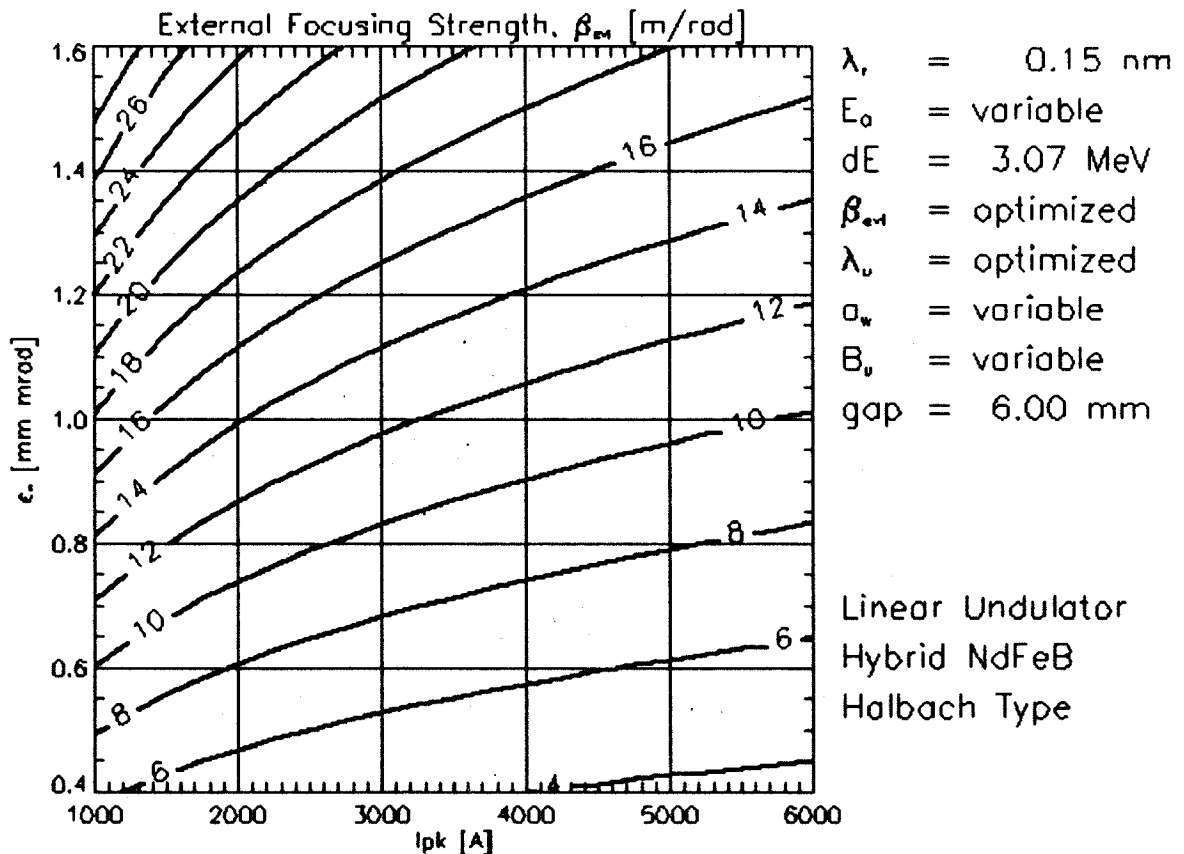
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Optimization Results - Focusing

$$\lambda_r = 0.15 \text{ nm}$$

linear

FEL Optimization



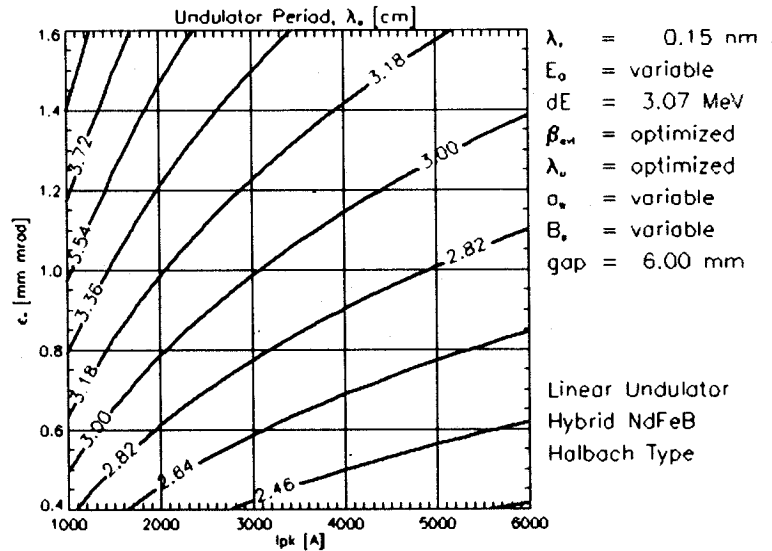
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - λ_u

$\lambda_r = 0.15$ nm
linear

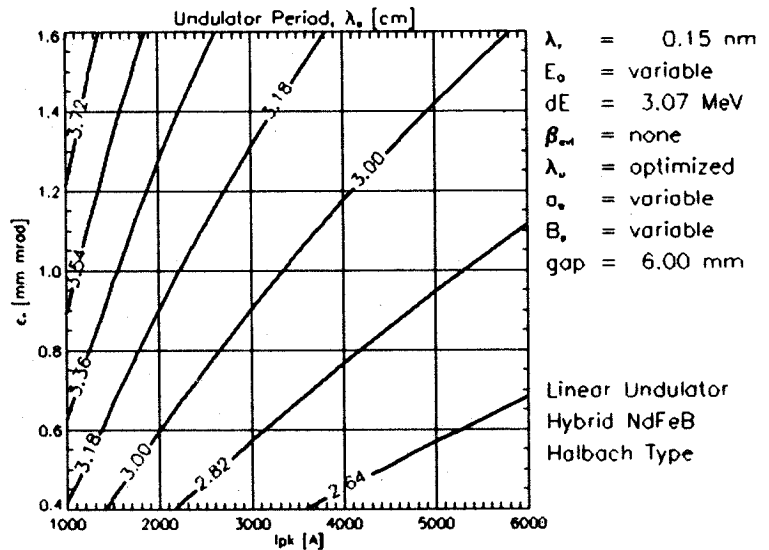
FEL Optimization



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FEL Optimization



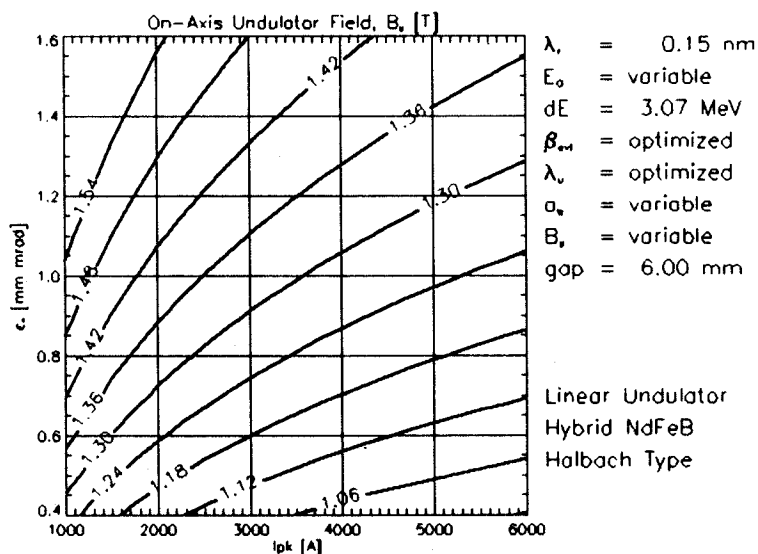
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - B_u

$\lambda_r = 0.15$ nm
linear

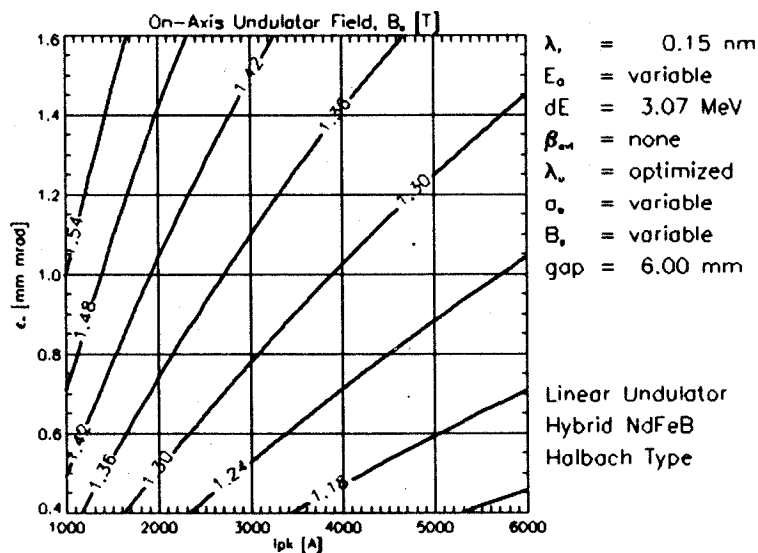
FEL Optimization



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FEL Optimization



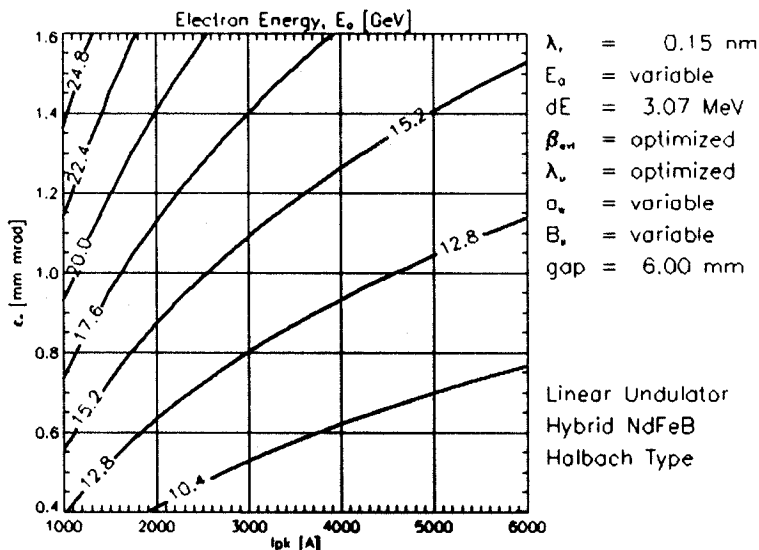
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - Energy

FEL Optimization

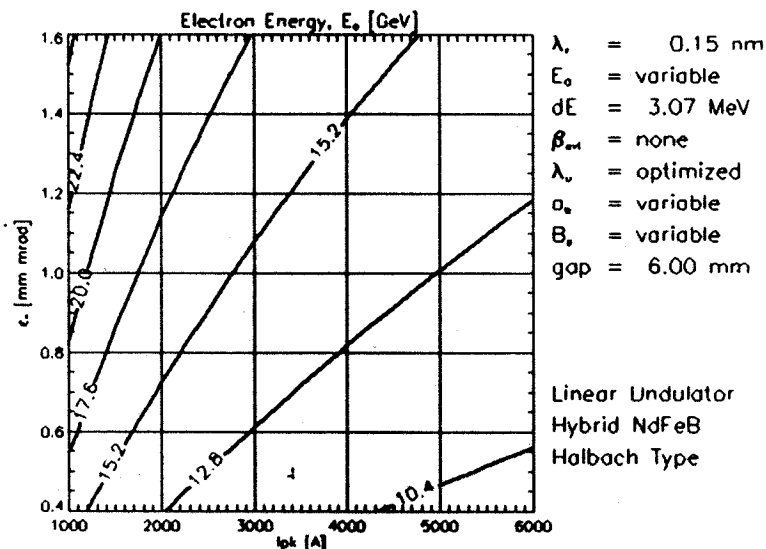
$\lambda_r = 0.15$ nm
linear



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FEL Optimization



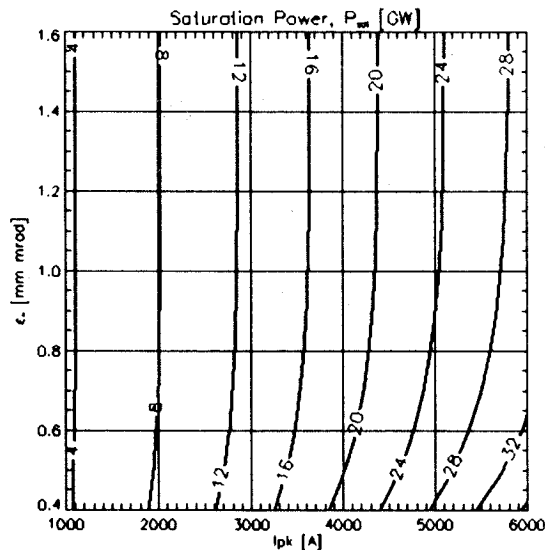
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - P_{sat}

$\lambda_r = 0.15$ nm
linear

FEL Optimization



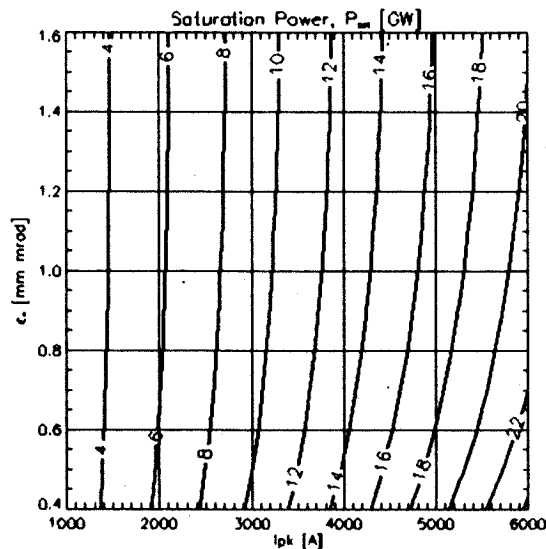
$\lambda_r = 0.15$ nm
 $E_0 =$ variable
 $dE = 3.07$ MeV
 $\beta_{\text{ext}} =$ optimized
 $\lambda_u =$ optimized
 $a_u =$ variable
 $B_u =$ variable
gap = 6.00 mm

Linear Undulator
Hybrid NdFeB
Halbach Type

Based on: M. Xie, PAC95, p. 183 (1996)

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FEL Optimization



$\lambda_r = 0.15$ nm
 $E_0 =$ variable
 $dE = 3.07$ MeV
 $\beta_{\text{ext}} =$ none
 $\lambda_u =$ optimized
 $a_u =$ variable
 $B_u =$ variable
gap = 6.00 mm

Linear Undulator
Hybrid NdFeB
Halbach Type

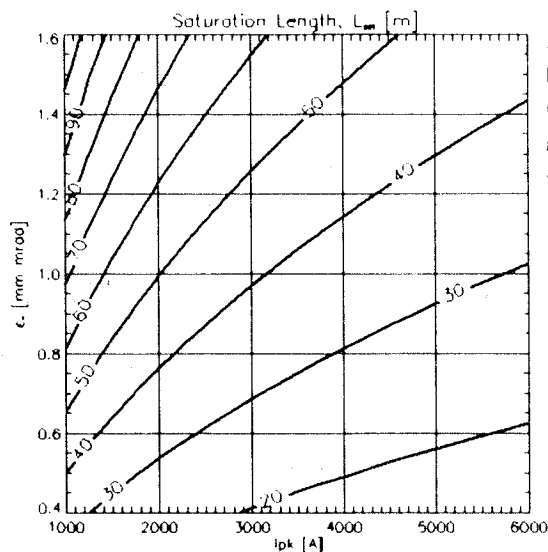
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - L_{sat}

FEL Optimization

$\lambda_r = 0.15$ nm
helical



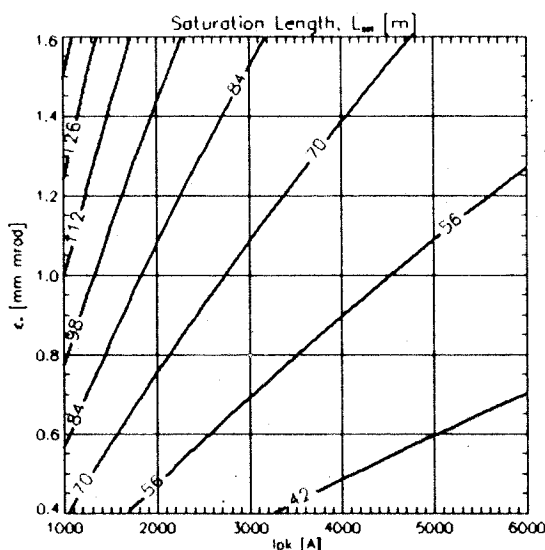
$\lambda_r = 0.15$ nm
 $E_0 =$ variable
 $dE = 3.07$ MeV
 $\beta_{\text{ext}} =$ optimized
 $\lambda_u =$ optimized
 $a_u =$ variable
 $B_u =$ variable
dia. = 12.50 mm

Helical Undulator
Superconducting
Shlomo Caspi Type

Based on: M. Xie, PAC95, p. 183 (1996)

H.-D. Nuhn, SLAC / SSRL

FEL Optimization



$\lambda_r = 0.15$ nm
 $E_0 =$ variable
 $dE = 3.07$ MeV
 $\beta_{\text{ext}} =$ none
 $\lambda_u =$ optimized
 $a_u =$ variable
 $B_u =$ variable
dia. = 12.50 mm

Helical Undulator
Superconducting
Shlomo Caspi Type

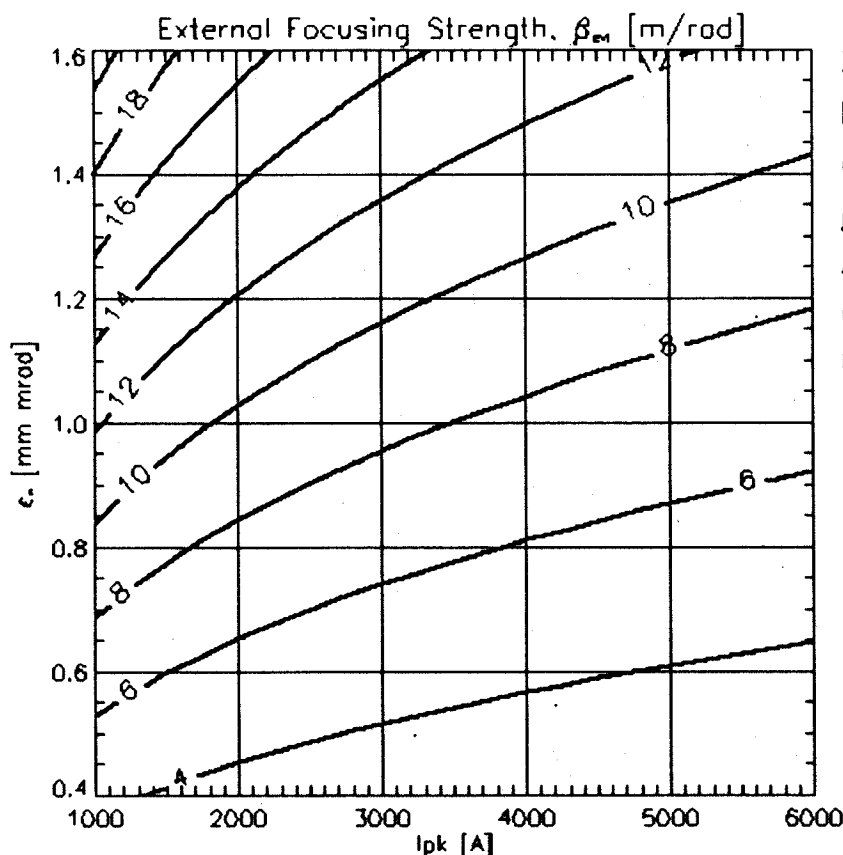
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - Focusing

$\lambda_r = 0.15$ nm
helical

FEL Optimization



$\lambda_r = 0.15$ nm
 $E_o =$ variable
 $dE = 3.07$ MeV
 $\beta_{ext} =$ optimized
 $\lambda_u =$ optimized
 $\alpha_w =$ variable
 $B_u =$ variable
dia. = 12.50 mm

Helical Undulator
Superconducting
Shlomo Caspi Type

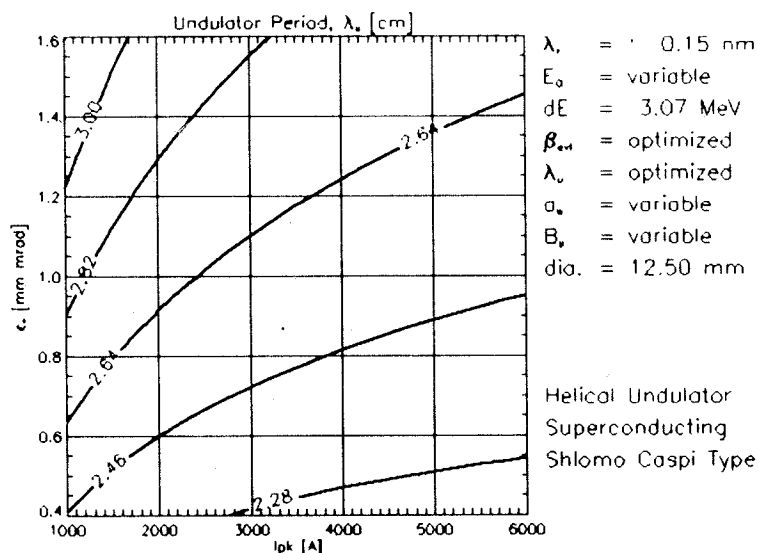
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - λ_u

FEL Optimization

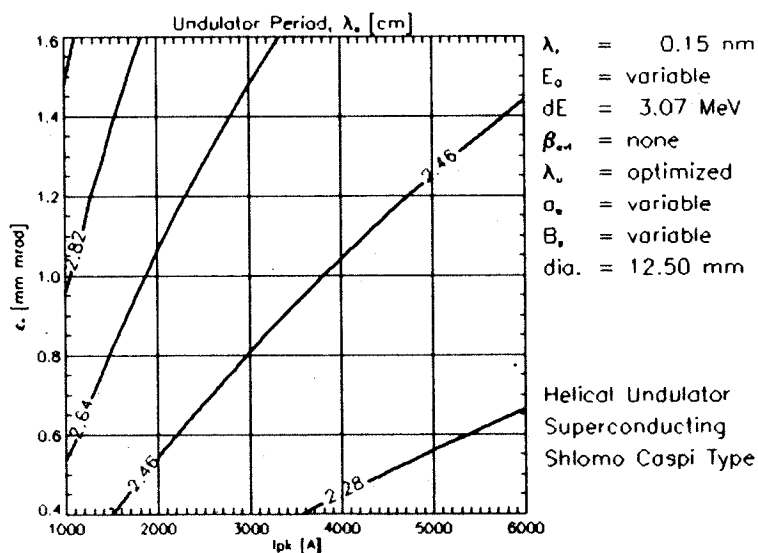
$\lambda_r = 0.15$ nm
helical



Based on: M. Xie, PAC95, p. 183 (1996)

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FEL Optimization



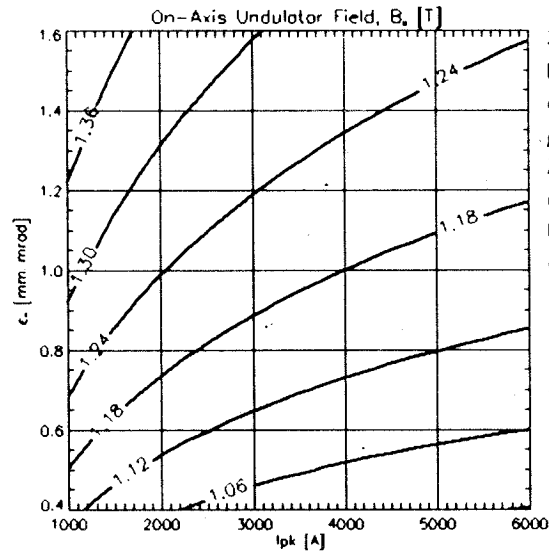
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - B_u

FEL Optimization

$\lambda_r = 0.15$ nm
helical



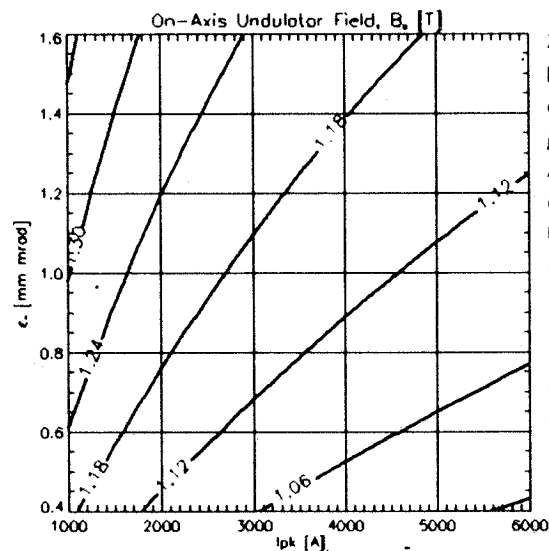
$\lambda_r = 0.15$ nm
 $E_o =$ variable
 $dE = 3.07$ MeV
 $\beta_{w,0} =$ optimized
 $\lambda_w =$ optimized
 $a_w =$ variable
 $B_u =$ variable
dia. = 12.50 mm

Helical Undulator
Superconducting
Shlomo Caspi Type

Based on: M. Xie, PAC95, p. 183 (1996)

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FEL Optimization



$\lambda_r = 0.15$ nm
 $E_o =$ variable
 $dE = 3.07$ MeV
 $\beta_{w,0} =$ none
 $\lambda_w =$ optimized
 $a_w =$ variable
 $B_u =$ variable
dia. = 12.50 mm

Helical Undulator
Superconducting
Shlomo Caspi Type

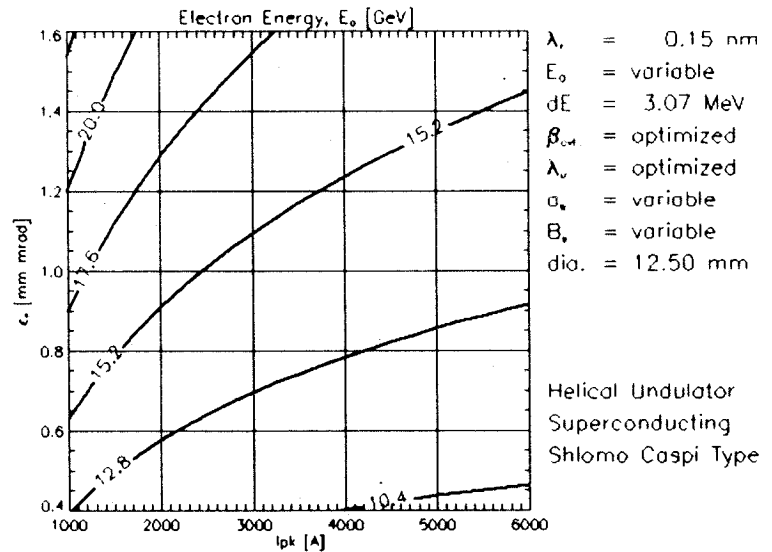
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - Energy

$\lambda_r = 0.15$ nm
helical

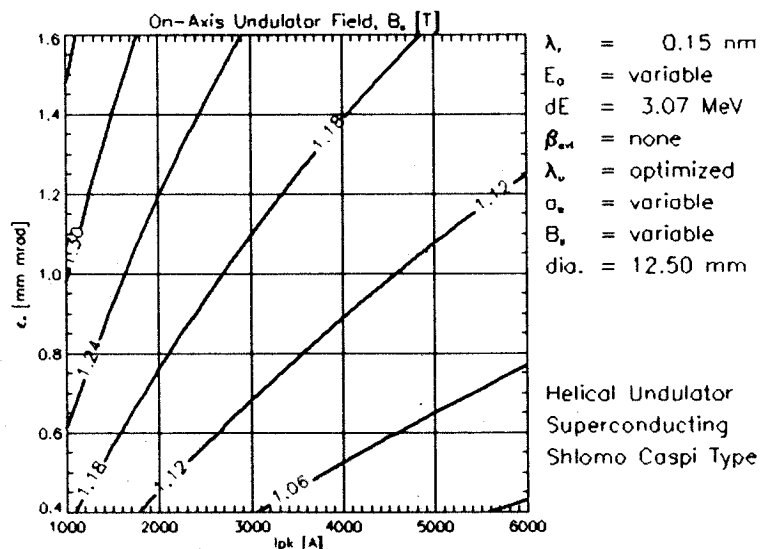
FEL Optimization



Based on: M. Xie, PAC95, p. 183 (1996)

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FEL Optimization



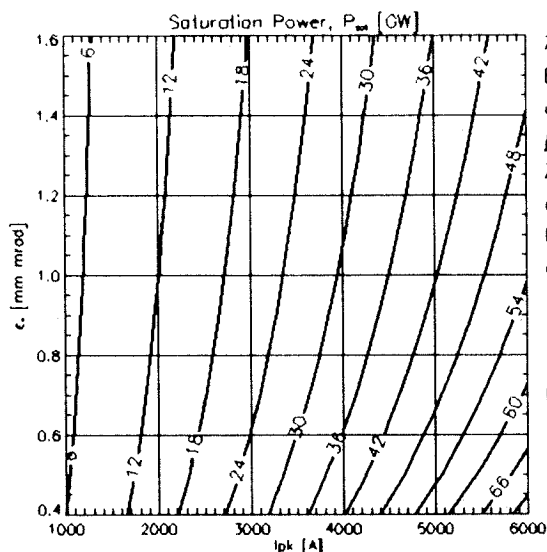
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - P_{sat}

FEL Optimization

$\lambda_r = 0.15$ nm
helical



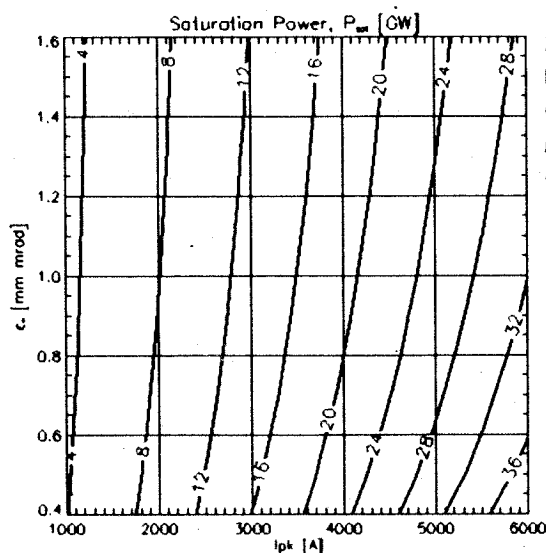
$\lambda_r = 0.15$ nm
 $E_0 =$ variable
 $dE = 3.07$ MeV
 $\beta_{\text{ext}} =$ optimized
 $\lambda_w =$ optimized
 $a_w =$ variable
 $B_w =$ variable
dia. = 12.50 mm

Helical Undulator
Superconducting
Shlomo Caspi Type

Based on: M. Xie, PAC95, p. 183 (1996)

H.-D. Nuhn, SLAC / SSRL

FEL Optimization



$\lambda_r = 0.15$ nm
 $E_0 =$ variable
 $dE = 3.07$ MeV
 $\beta_{\text{ext}} =$ none
 $\lambda_w =$ optimized
 $a_w =$ variable
 $B_w =$ variable
dia. = 12.50 mm

Helical Undulator
Superconducting
Shlomo Caspi Type

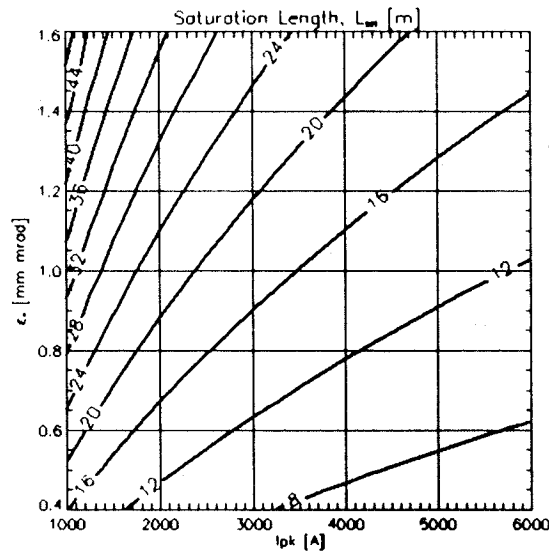
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - L_{sat}

FEL Optimization

$\lambda_r = 1.5 \text{ nm}$
linear



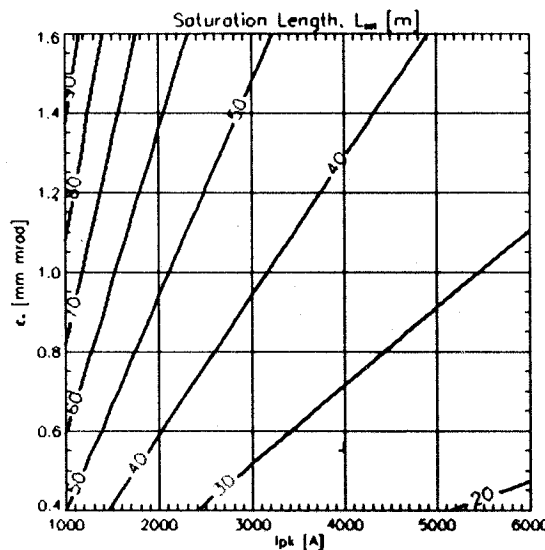
$\lambda_r = 1.50 \text{ nm}$
 $E_0 = \text{variable}$
 $dE = 3.07 \text{ MeV}$
 $\beta_{\text{ext}} = \text{optimized}$
 $\lambda_u = \text{optimized}$
 $a_w = \text{variable}$
 $B_w = \text{variable}$
 $\text{gap} = 6.00 \text{ mm}$

Linear Undulator
Hybrid NdFeB
Halbach Type

Based on: M. Xie, PAC95, p. 183 (1996)

H.-D. Nuhn, SLAC / SSRL

FEL Optimization



$\lambda_r = 1.50 \text{ nm}$
 $E_0 = \text{variable}$
 $dE = 3.07 \text{ MeV}$
 $\beta_{\text{ext}} = \text{none}$
 $\lambda_u = \text{optimized}$
 $a_w = \text{variable}$
 $B_w = \text{variable}$
 $\text{gap} = 6.00 \text{ mm}$

Linear Undulator
Hybrid NdFeB
Halbach Type

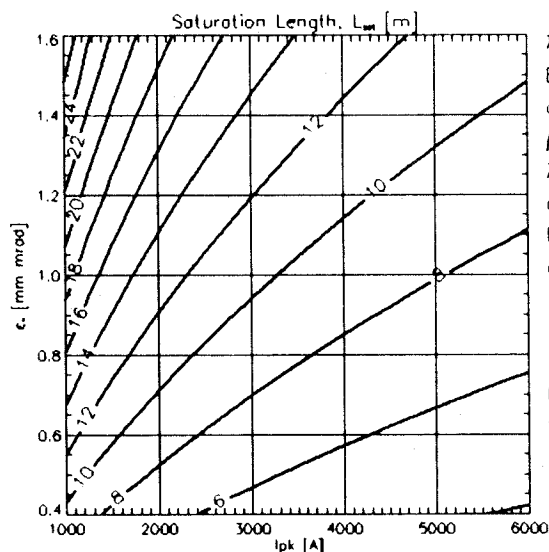
Based on: M. Xie, PAC95, p. 183 (1996)

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Optimization Results - L_{sat}

FEL Optimization

$\lambda_r = 15 \text{ nm}$
helical



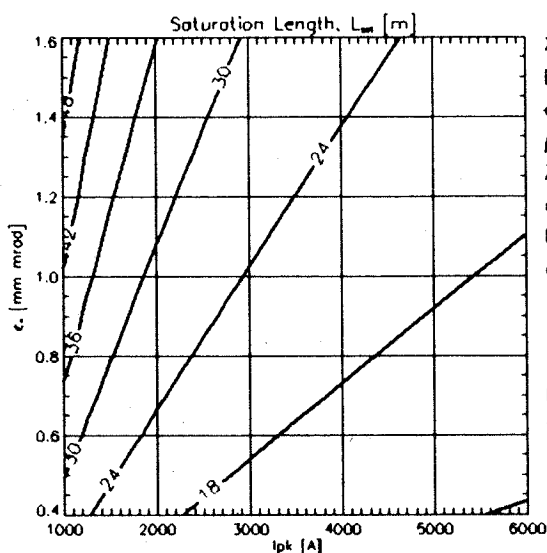
$\lambda_r = 1.50 \text{ nm}$
 $E_0 = \text{variable}$
 $dE = 3.07 \text{ MeV}$
 $\beta_{\text{ext}} = \text{optimized}$
 $\lambda_u = \text{optimized}$
 $a_u = \text{variable}$
 $B_u = \text{variable}$
 $\text{dia.} = 12.50 \text{ mm}$

Helical Undulator
Superconducting
Shlomo Caspi Type

Based on: M. Xie, PAC95, p. 183 (1996)

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FEL Optimization



$\lambda_r = 1.50 \text{ nm}$
 $E_0 = \text{variable}$
 $dE = 3.07 \text{ MeV}$
 $\beta_{\text{ext}} = \text{none}$
 $\lambda_u = \text{optimized}$
 $a_u = \text{variable}$
 $B_u = \text{variable}$
 $\text{dia.} = 12.50 \text{ mm}$

Helical Undulator
Superconducting
Shlomo Caspi Type

Based on: M. Xie, PAC95, p. 183 (1996)

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Comparison with Simulations

FEL Optimization

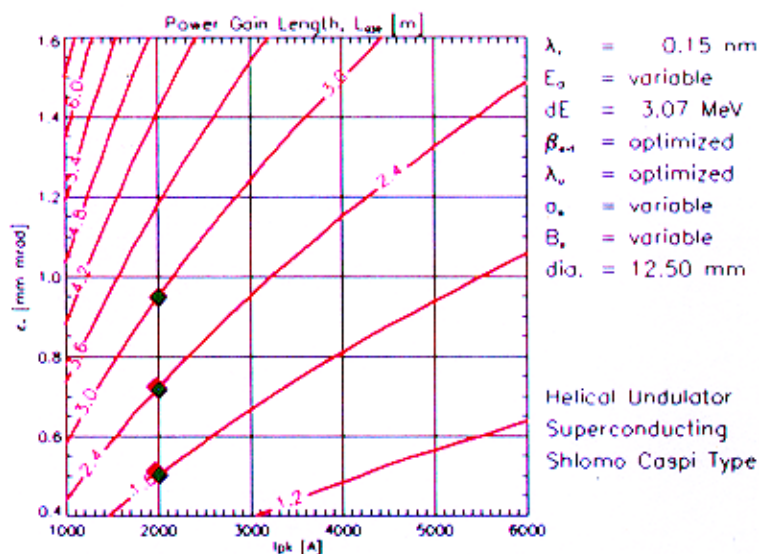
$$\lambda_r = 0.15 \text{ nm}$$

GINGER Simulation Results:

$$\epsilon_n = 0.950 \text{ mm mrad}, L_G = 3.070 \text{ m}$$

$$\epsilon_n = 0.724 \text{ mm mrad}, L_G = 2.426 \text{ m}$$

$$\epsilon_n = 0.504 \text{ mm mrad}, L_G = 1.876 \text{ m}$$



Based on: M. Xie, PAC95, p. 183 (1996)

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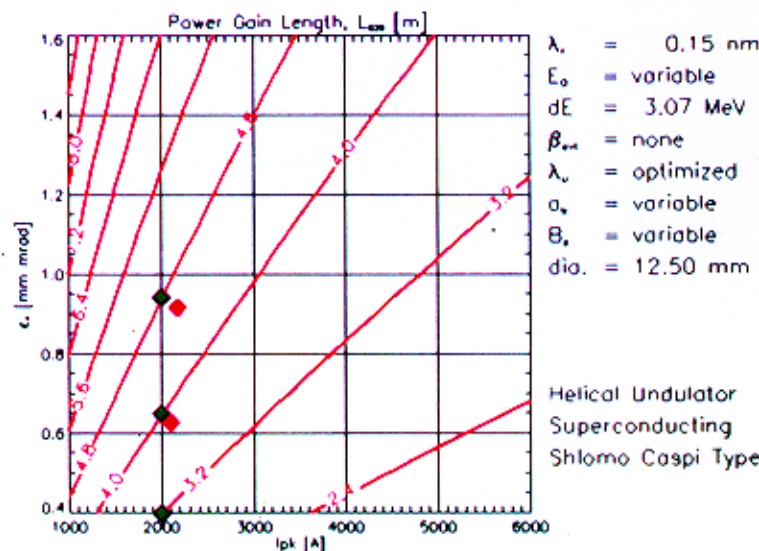
FEL Optimization

GINGER Simulation Results:

$$\epsilon_n = 0.936 \text{ mm mrad}, L_G = 4.571 \text{ m}$$

$$\epsilon_n = 0.645 \text{ mm mrad}, L_G = 3.885 \text{ m}$$

$$\epsilon_n = 0.398 \text{ mm mrad}, L_G = 3.208 \text{ m}$$



Based on: M. Xie, PAC95, p. 183 (1996)

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Comparison with Simulations

$$\lambda_r = 1.5 \text{ nm}$$

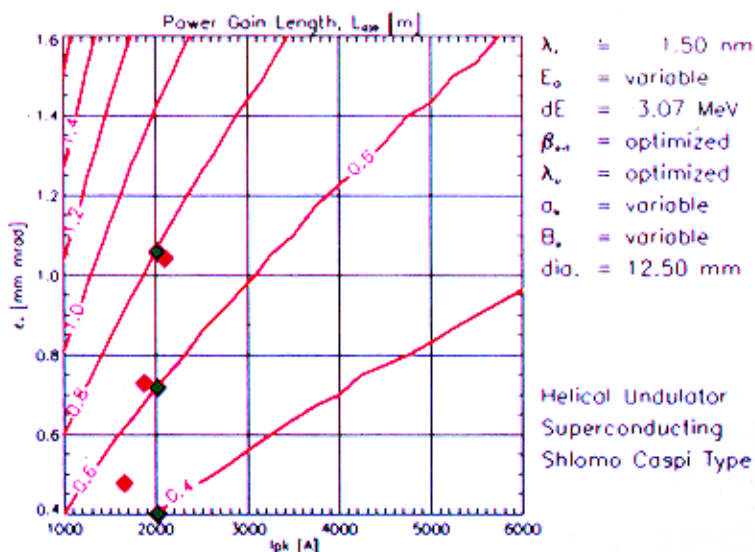
GINGER Simulation Results:

$$\epsilon_n = 1.059 \text{ mm mrad}, L_G = 0.783 \text{ m}$$

$$\epsilon_n = 0.718 \text{ mm mrad}, L_G = 0.640 \text{ m}$$

$$\epsilon_n = 0.402 \text{ mm mrad}, L_G = 0.516 \text{ m}$$

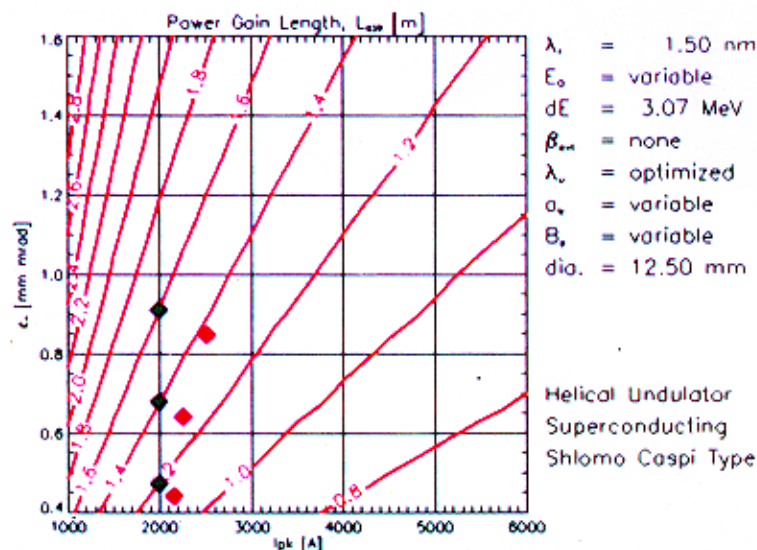
FEL Optimization



Based on: M. Xie, PAC95, p. 183 (1996)

H.-D. Nuhn, SLAC / SSRL

FEL Optimization



Based on: M. Xie, PAC95, p. 183 (1996)

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Sensitivities to Parameter Changes

$g = 12.5$ mm, $a_w = 3.06$, $\varepsilon_n = 0.95$ mm mrad, $I_{pk} = 2000$ A, $\lambda_r = 1.5$ Å,
 $\lambda_u = 2.66$ cm, $\gamma = 30283$, $\sigma_\gamma = 6$, $\beta_{xy} = 9.1$ m, $L_{sat} = 48.1$ m, $P_{sat} = 12.1$ GW

Sensitivity of Saturation Power
and Length Parameter x:
Helical Undulator.

$$\frac{\Delta P_{sat} / P_{sat}}{\Delta x / x}$$

$$\frac{\Delta L_{sat} / L_{sat}}{\Delta x / x}$$

	P_{sat}	L_{sat}	var	const							
λ_r	0.54	-0.61	γ	λ_u	γ	g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}
λ_r	1.61	-0.85	g a_w	λ_u	γ			σ_γ	ε_n	I_{pk}	β_{ext}
λ_u	6.68	-2.74	λ_r		γ	g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}
λ_u	4.26	0.00	γ	λ_r		g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}
λ_u	-0.50	1.06	g a_w	λ_r	γ			σ_γ	ε_n	I_{pk}	β_{ext}
γ	-1.08	1.23	λ_r	λ_u		g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}
γ	2.13	-0.47	g a_w	λ_r	λ_u			σ_γ	ε_n	I_{pk}	β_{ext}
g	-4.58	2.42	λ_r a_w	λ_u	γ			σ_γ	ε_n	I_{pk}	β_{ext}
g	-3.04	0.68	γ a_w	λ_r	λ_u			σ_γ	ε_n	I_{pk}	β_{ext}
σ_γ	-0.29	0.06		λ_r	λ_u	γ	g	a_w	ε_n	I_{pk}	β_{ext}
ε_n	-1.52	0.85		λ_r	λ_u	γ	g	a_w	σ_γ	I_{pk}	β_{ext}
I_{pk}	1.86	-0.50		λ_r	λ_u	γ	g	a_w	σ_γ	ε_n	β_{ext}
β_{ext}	0.42	0.00		λ_r	λ_u	γ	g	a_w	σ_γ	ε_n	I_{pk}

ba

Sensitivities to Parameter Changes

$g = 12.5$ mm, $a_w = 2.48$, $\epsilon_n = 0.5$ mm mrad, $I_{pk} = 2000$ A, $\lambda_r = 1.5$ Å,
 $\lambda_u = 2.4$ cm, $\gamma = 23906$, $\sigma_\gamma = 6$, $\beta_{xy} = 4.5$ m, $L_{sat} = 28.5$ m, $P_{sat} = 14.5$ GW

Sensitivity of Saturation Power
and Length Parameter x :
Helical Undulator.

$$\frac{\Delta P_{sat} / P_{sat}}{\Delta x / x}$$

$$\frac{\Delta L_{sat} / L_{sat}}{\Delta x / x}$$

	P_{sat}	L_{sat}	var	const									
λ_r	0.49	-0.59	γ	λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_r	1.53	-0.82	g a_w	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	6.58	-2.76	λ_r		γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	4.28	0.00	γ	λ_r		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	-0.56	1.09	g a_w	λ_r	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
γ	-0.98	1.18	λ_r	λ_u		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
γ	2.07	-0.47	g a_w	λ_r	λ_u			σ_γ	ϵ_n	I_{pk}	β_{ext}		
g	-4.55	2.45	λ_r a_w	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
g	-3.08	0.69	γ a_w	λ_r	λ_u			σ_γ	ϵ_n	I_{pk}	β_{ext}		
σ_γ	-0.24	0.04		λ_r	λ_u	γ	g	a_w	ϵ_n	I_{pk}	β_{ext}		
ϵ_n	-1.40	0.80		λ_r	λ_u	γ	g	a_w	σ_γ	I_{pk}	β_{ext}		
I_{pk}	1.84	-0.49		λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n	β_{ext}		
β_{ext}	0.43	0.00		λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}		

bc

Sensitivities to Parameter Changes

$g = 12.5$ mm, $a_w = 2.93$, $\varepsilon_n = 0.936$ mm mrad, $I_{pk} = 2000$ A, $\lambda_r = 1.5$ Å,
 $\lambda_u = 2.60$ cm, $\gamma = 28824$, $\sigma_\gamma = 6$, $\beta_{xy} = \text{none}$, $L_{sat} = 77.9$ m, $P_{sat} = 8.0$ GW

Sensitivity of Saturation Power
and Length Parameter x:
Helical Undulator.

$$\frac{\Delta P_{sat} / P_{sat}}{\Delta x / x}$$

$$\frac{\Delta L_{sat} / L_{sat}}{\Delta x / x}$$

	P_{sat}	L_{sat}	var	const							
λ_r	-0.01	-0.46	γ	λ_u	γ	g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}
λ_r	1.14	-0.75	g a_w	λ_u	γ			σ_γ	ε_n	I_{pk}	β_{ext}
λ_u	4.76	-2.10	λ_r		γ	g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}
λ_u	4.80	0.00	γ	λ_r		g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}
λ_u	-0.40	1.30	g a_w	λ_r	γ			σ_γ	ε_n	I_{pk}	β_{ext}
γ	0.02	0.93	λ_r	λ_u		g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}
γ	2.31	-0.58	g a_w	λ_r	λ_u			σ_γ	ε_n	I_{pk}	β_{ext}
g	-3.29	2.17	λ_r a_w	λ_u	γ			σ_γ	ε_n	I_{pk}	β_{ext}
g	-3.32	0.83	γ a_w	λ_r	λ_u			σ_γ	ε_n	I_{pk}	β_{ext}
σ_γ	-1.09	0.41		λ_r	λ_u	γ	g	a_w	ε_n	I_{pk}	β_{ext}
ε_n	-0.74	0.51		λ_r	λ_u	γ	g	a_w	σ_γ	I_{pk}	β_{ext}
I_{pk}	1.76	-0.46		λ_r	λ_u	γ	g	a_w	σ_γ	ε_n	β_{ext}
β_{ext}				λ_r	λ_u	γ	g	a_w	σ_γ	ε_n	I_{pk}

bd

Sensitivities to Parameter Changes

$g = 12.5$ mm, $a_w = 2.47$, $\epsilon_n = 0.398$ mm mrad, $I_{pk} = 2000$ A, $\lambda_r = 1.5$ Å,
 $\lambda_u = 2.39$ cm, $\gamma = 23810$, $\sigma_\gamma = 6$, $\beta_{xy} = \text{none}$, $L_{sat} = 51.6$ m, $P_{sat} = 9.5$ GW

Sensitivity of Saturation Power
and Length Parameter x:
Helical Undulator.

$$\frac{\Delta P_{sat} / P_{sat}}{\Delta x / x}$$

$$\frac{\Delta L_{sat} / L_{sat}}{\Delta x / x}$$

	P_{sat}	L_{sat}	var	const									
λ_r	-0.05	-0.45	γ	λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_r	1.07	-0.73	g a_w	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	4.54	-2.09	λ_r		γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	4.78	0.00	γ	λ_r		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	-0.45	1.34	g a_w	λ_r	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
γ	0.10	0.89	λ_r	λ_u		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
γ	2.24	-0.57	g a_w	λ_r	λ_u			σ_γ	ϵ_n	I_{pk}	β_{ext}		
g	-3.18	2.18	λ_r a_w	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
g	-3.33	0.85	γ a_w	λ_r	λ_u			σ_γ	ϵ_n	I_{pk}	β_{ext}		
σ_γ	-1.01	0.38		λ_r	λ_u	γ	g	a_w	ϵ_n	I_{pk}	β_{ext}		
ϵ_n	-0.62	0.46		λ_r	λ_u	γ	g	a_w	σ_γ	I_{pk}	β_{ext}		
I_{pk}	1.72	-0.44		λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n	β_{ext}		
β_{ext}													

bf

Sensitivities to Parameter Changes

$g = 12.5$ mm, $a_w = 2.47$, $\epsilon_n = 0.398$ mm mrad, $I_{pk} = 2000$ A, $\lambda_r = 1.5$ Å,
 $\lambda_u = 2.39$ cm, $\gamma = 23810$, $\sigma_\gamma = 6$, $\beta_{xy} = \text{none}$, $L_{sat} = 51.6$ m, $P_{sat} = 9.5$ GW

Sensitivity of Saturation Power
 and Length Parameter x :
 Helical Undulator.

$$\frac{\Delta P_{sat}}{P_{sat}} / \frac{\Delta x}{x}$$

$$\frac{\Delta L_{sat}}{L_{sat}} / \frac{\Delta x}{x}$$

	P_{sat}	L_{sat}	var	const									
λ_r	-0.05	-0.45	γ	λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_r	1.07	-0.73	g a_w	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	4.54	-2.09	λ_r		γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	4.78	0.00	γ	λ_r		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	-0.45	1.34	g a_w	λ_r	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
γ	0.10	0.89	λ_r	λ_u		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
γ	2.24	-0.57	g a_w	λ_r	λ_u			σ_γ	ϵ_n	I_{pk}	β_{ext}		
g	-3.18	2.18	λ_r a_w	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
g	-3.33	0.85	γ a_w	λ_r	λ_u			σ_γ	ϵ_n	I_{pk}	β_{ext}		
σ_γ	-1.01	0.38		λ_r	λ_u	γ	g	a_w	ϵ_n	I_{pk}	β_{ext}		
ϵ_n	-0.62	0.46		λ_r	λ_u	γ	g	a_w	σ_γ	I_{pk}	β_{ext}		
I_{pk}	1.72	-0.44		λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n	β_{ext}		
β_{ext}													

bf

Sensitivities to Parameter Changes

$g = 12.5$ mm, $a_w = 2.74$, $\epsilon_n = 1.06$ mm mrad, $I_{pk} = 2000$ A, $\lambda_r = 15.0$ Å,
 $\lambda_u = 2.51$ cm, $\gamma = 8438$, $\sigma_\gamma = 6$, $\beta_{xy} = 1.3$ m, $L_{sat} = 13.5$ m, $P_{sat} = 11.1$ GW

Sensitivity of Saturation Power
and Length Parameter x:
Helical Undulator.

$$\frac{\Delta P_{sat}}{P_{sat}} / \frac{\Delta x}{x}$$

$$\frac{\Delta L_{sat}}{L_{sat}} / \frac{\Delta x}{x}$$

	P_{sat}	L_{sat}	var	const									
λ_r	0.42	-0.56	γ	λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_r	1.47	-0.80	g a_w	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	6.17	-2.58	λ_r		γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	4.24	0.00	γ	λ_r		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
λ_u	-0.54	1.08	g a_w	λ_r	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
γ	-0.84	1.13	λ_r	λ_u		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}		
γ	2.09	-0.47	g a_w	λ_r	λ_u			σ_γ	ϵ_n	I_{pk}	β_{ext}		
g	-4.28	2.33	λ_r a_w	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}		
g	-3.05	0.69	γ a_w	λ_r	λ_u			σ_γ	ϵ_n	I_{pk}	β_{ext}		
σ_γ	-0.42	0.13		λ_r	λ_u	γ	g	a_w	ϵ_n	I_{pk}	β_{ext}		
ϵ_n	-1.35	0.78		λ_r	λ_u	γ	g	a_w	σ_γ	I_{pk}	β_{ext}		
I_{pk}	1.92	-0.53		λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n	β_{ext}		
β_{ext}	0.42	0.00		λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}		

Sensitivities to Parameter Changes

$g = 12.5 \text{ mm}$, $a_w = 3.02$, $\varepsilon_n = 0.913 \text{ mm mrad}$, $I_{pk} = 2000 \text{ A}$, $\lambda_r = 15.0 \text{ \AA}$,
 $\lambda_u = 2.64 \text{ cm}$, $\gamma = 9435$, $\sigma_\gamma = 6$, $\beta_{xy} = \text{none}$, $L_{sat} = 27.7 \text{ m}$, $P_{sat} = 7.6 \text{ GW}$

Sensitivity of Saturation Power

and Length Parameter x:

Helical Undulator.

$$\frac{\Delta P_{sat}}{P_{sat}} / \frac{\Delta x}{x}$$

$$\frac{\Delta L_{sat}}{L_{sat}} / \frac{\Delta x}{x}$$

	P_{sat}	L_{sat}	var	const									
λ_r	-0.11	-0.42	γ	λ_u	γ	g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}		
λ_r	1.05	-0.72	g a_w	λ_u	γ			σ_γ	ε_n	I_{pk}	β_{ext}		
λ_u	4.28	-1.90	λ_r		γ	g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}		
λ_u	4.76	0.00	γ	λ_r		g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}		
λ_u	-0.42	1.31	g a_w	λ_r	γ			σ_γ	ε_n	I_{pk}	β_{ext}		
γ	0.22	0.85	λ_r	λ_u		g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}		
γ	2.32	-0.59	g a_w	λ_r	λ_u			σ_γ	ε_n	I_{pk}	β_{ext}		
g	-3.00	2.04	λ_r a_w	λ_u	γ			σ_γ	ε_n	I_{pk}	β_{ext}		
g	-3.30	0.84	γ a_w	λ_r	λ_u			σ_γ	ε_n	I_{pk}	β_{ext}		
σ_γ	-1.28	0.51		λ_r	λ_u	γ	g	a_w	ε_n	I_{pk}	β_{ext}		
ε_n	-0.63	0.46		λ_r	λ_u	γ	g	a_w	σ_γ	I_{pk}	β_{ext}		
I_{pk}	1.84	-0.50		λ_r	λ_u	γ	g	a_w	σ_γ	ε_n	β_{ext}		
β_{ext}													

cd

Sensitivities to Parameter Changes

$g = 12.5 \text{ mm}$, $a_w = 2.09$, $\varepsilon_n = 0.402 \text{ mm mrad}$, $I_{pk} = 2000 \text{ A}$, $\lambda_r = 15.0 \text{ \AA}$,
 $\lambda_u = 2.2 \text{ cm}$, $\gamma = 6300$, $\sigma_\gamma = 6$, $\beta_{xy} = 0.45 \text{ m}$, $L_{sat} = 6.6 \text{ m}$, $P_{sat} = 13.9 \text{ GW}$

Sensitivity of Saturation Power
 and Length Parameter x:
 Helical Undulator.

$$\frac{\Delta P_{sat} / P_{sat}}{\Delta x / x}$$

$$\frac{\Delta L_{sat} / L_{sat}}{\Delta x / x}$$

	P_{sat}	L_{sat}	var	const									
λ_r	0.36	-0.54	γ	λ_u	γ	g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}		
λ_r	1.37	-0.77	g a_w	λ_u	γ			σ_γ	ε_n	I_{pk}	β_{ext}		
λ_u	5.97	-2.58	λ_r		γ	g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}		
λ_u	4.22	0.00	γ	λ_r		g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}		
λ_u	-0.62	1.13	g a_w	λ_r	γ			σ_γ	ε_n	I_{pk}	β_{ext}		
γ	-0.73	1.07	λ_r	λ_u		g	a_w	σ_γ	ε_n	I_{pk}	β_{ext}		
γ	2.01	-0.47	g a_w	λ_r	λ_u			σ_γ	ε_n	I_{pk}	β_{ext}		
g	-4.20	2.36	λ_r a_w	λ_u	γ			σ_γ	ε_n	I_{pk}	β_{ext}		
g	-3.08	0.72	γ a_w	λ_r	λ_u			σ_γ	ε_n	I_{pk}	β_{ext}		
σ_γ	-0.31	0.08		λ_r	λ_u	γ	g	a_w	ε_n	I_{pk}	β_{ext}		
ε_n	-1.17	0.70		λ_r	λ_u	γ	g	a_w	σ_γ	I_{pk}	β_{ext}		
I_{pk}	1.87	-0.51		λ_r	λ_u	γ	g	a_w	σ_γ	ε_n	β_{ext}		
β_{ext}	0.42	0.00		λ_r	λ_u	γ	g	a_w	σ_γ	ε_n	I_{pk}		

Sensitivities to Parameter Changes

$g = 12.5$ mm, $a_w = 2.69$, $\epsilon_n = 0.476$ mm mrad, $I_{pk} = 2000$ A, $\lambda_r = 15.0$ Å,
 $\lambda_u = 2.49$ cm, $\gamma = 8278$, $\sigma_\gamma = 6$, $\beta_{xy} = \text{none}$, $L_{sat} = 20.7$ m, $P_{sat} = 8.6$ GW

Sensitivity of Saturation Power
 and Length Parameter x:
 Helical Undulator.

$$\frac{\Delta P_{sat} / P_{sat}}{\Delta x / x}$$

$$\frac{\Delta L_{sat} / L_{sat}}{\Delta x / x}$$

	P_{sat}	L_{sat}	var	const									
λ_r	-0.12	-0.42	γ	λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}	
λ_r	1.01	-0.70	$g a_w$	λ_r	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}	
λ_u	4.18	-1.91	λ_r		λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}	
λ_u	4.76	0.00	γ	λ_r	λ_u		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}	
λ_u	-0.43	1.32	$g a_w$	λ_r	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}	
γ	0.25	0.83	λ_r		λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}	
γ	2.26	-0.58	$g a_w$	λ_r	λ_u	γ			σ_γ	ϵ_n	I_{pk}	β_{ext}	
gap	-2.94	2.06	λ_r		λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}	
gap	-3.31	0.84	γ	λ_r	λ_u		g	a_w	σ_γ	ϵ_n	I_{pk}	β_{ext}	
σ_γ	-1.21	0.48		λ_r	λ_u	γ	g	a_w		ϵ_n	I_{pk}	β_{ext}	
ϵ_n	-0.57	0.44		λ_r	λ_u	γ	g	a_w	σ_γ		I_{pk}	β_{ext}	
I_{pk}	1.82	-0.49		λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n		β_{ext}	
β_{ext}				λ_r	λ_u	γ	g	a_w	σ_γ	ϵ_n	I_{pk}		

cf

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- **Thanks to Ilan Ben-Zvi for the suggestion for this presentation.**

Conclusion

- **FEL scenarios have been analyzed for an emittance range from 1.6 to 0.4 mm mrad using 3D analytic theory.**
- **Results compare well with multidimensional, polychromatic FEL simulation code, GINGER.**
- **Lower emittance reduces undulator length and energy requirements.**
- **Lower emittance can also be utilized to reduce peak current.**
- **Elimination of quadrupole focusing becomes an interesting option.**
- **Dependence of trajectory tolerances on smaller emittance is still to be studied.**